



STANDARDIZED

UXO TECHNOLOGY DEMONSTRATION SITE

BLIND GRID SCORING RECORD NO. 404

SITE LOCATION: U.S. ARMY ABERDEEN PROVING GROUND

> DEMONSTRATOR: SHAW, INC. 312 DIRECTOR'S DRIVE KNOXSVILLE, TN 37923

TECHNOLOGY TYPE/PLATFORM: UXO MAPPER/PUSHCART (DUAL SENSOR G858 MAGNETOMETER)

PREPARED BY:
U.S. ARMY ABERDEEN TEST CENTER
ABERDEEN PROVING GROUND, MD 21005-5059

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U.S. ARMY DEVELOPMENTAL TEST COMMAND ABERDEEN PROVING GROUND, MD 21005-5055

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SECTION 1. GENERAL INFORMATION

1.1 BACKGROUND

Technologies under development for the detection and discrimination of unexploded ordnance (UXO) require testing so that their performance can be characterized. To that end, Standardized Test Sites have been developed at Aberdeen Proving Ground (APG), Maryland and U.S. Army Yuma Proving Ground (YPG), Arizona. These test sites provide a diversity of geology, climate, terrain, and weather as well as diversity in ordnance and clutter. Testing at these sites is independently administered and analyzed by the government for the purposes of characterizing technologies, tracking performance with system development, comparing performance of different systems, and comparing performance in different environments.

The Standardized UXO Technology Demonstration Site Program is a multi-agency program spearheaded by the U.S. Army Environmental Center (AEC). The U.S. Army Aberdeen Test Center (ATC) and the U.S. Army Corps of Engineers Engineering Research and Development Center (ERDC) provide programmatic support. The program is being funded and supported by the Environmental Security Technology Certification Program (ESTCP), the Strategic Environmental Research and Development Program (SERDP) and the Army Environmental Quality Technology Program (EQT).

1.2 SCORING OBJECTIVES

The objective in the Standardized UXO Technology Demonstration Site Program is to evaluate the detection and discrimination capabilities of a given technology under various field and soil conditions. Inert munitions and clutter items are positioned in various orientations and depths in the ground.

The evaluation objectives are as follows:

- a. To determine detection and discrimination effectiveness under realistic scenarios that vary targets, geology, clutter, topography, and vegetation.
 - b. To determine cost, time, and manpower requirements to operate the technology.
- c. To determine demonstrator's ability to analyze survey data in a timely manner and provide prioritized "Target Lists" with associated confidence levels.
- d. To provide independent site management to enable the collection of high quality, ground-truth, geo-referenced data for post-demonstration analysis.

1.2.1 Scoring Methodology

a. The scoring of the demonstrator's performance is conducted in two stages. These two stages are termed the RESPONSE STAGE and DISCRIMINATION STAGE. For both stages, the probability of detection (P_d) and the false alarms are reported as receiver-operating

characteristic (ROC) curves. False alarms are divided into those anomalies that correspond to emplaced clutter items, measuring the probability of false positive (P_{fp}), and those that do not correspond to any known item, termed background alarms.

- b. The RESPONSE STAGE scoring evaluates the ability of the system to detect emplaced targets without regard to ability to discriminate ordnance from other anomalies. For the blind grid RESPONSE STAGE, the demonstrator provides the scoring committee with a target response from each and every grid square along with a noise level below which target responses are deemed insufficient to warrant further investigation. This list is generated with minimal processing and, since a value is provided for every grid square, will include signals both above and below the system noise level.
- c. The DISCRIMINATION STAGE evaluates the demonstrator's ability to correctly identify ordnance as such and to reject clutter. For the blind grid DISCRIMINATION STAGE, the demonstrator provides the scoring committee with the output of the algorithms applied in the discrimination-stage processing for each grid square. The values in this list are prioritized based on the demonstrator's determination that a grid square is likely to contain ordnance. Thus, higher output values are indicative of higher confidence that an ordnance item is present at the specified location. For digital signal processing, priority ranking is based on algorithm output. For other discrimination approaches, priority ranking is based on human (subjective) judgment. The demonstrator also specifies the threshold in the prioritized ranking that provides optimum performance, (i.e., that is expected to retain all detected ordnance and rejects the maximum amount of clutter).
- d. The demonstrator is also scored on EFFICIENCY and REJECTION RATIO, which measures the effectiveness of the discrimination stage processing. The goal of discrimination is to retain the greatest number of ordnance detections from the anomaly list, while rejecting the maximum number of anomalies arising from non-ordnance items. EFFICIENCY measures the fraction of detected ordnance retained after discrimination, while the REJECTION RATIO measures the fraction of false alarms rejected. Both measures are defined relative to performance at the demonstrator-supplied level below which all responses are considered noise, i.e., the maximum ordnance detectable by the sensor and its accompanying false positive rate or background alarm rate.
- e. All scoring factors are generated utilizing the Standardized UXO Probability and Plot Program, version 3.1.1.

1.2.2 Scoring Factors

Factors to be measured and evaluated as part of this demonstration include:

- a. Response Stage ROC curves:
- (1) Probability of Detection (P_d res).
- (2) Probability of False Positive (P_{fp} res).
- (3) Background Alarm Rate (BAR^{res}) or Probability of Background Alarm (P_{BA}^{res}).

- b. Discrimination Stage ROC curves:
- (1) Probability of Detection (P_d disc).
- (2) Probability of False Positive (P_{fp}^{disc}) .
- (3) Background Alarm Rate (BAR^{disc}) or Probability of Background Alarm (P_{BA}^{disc}).
- c. Metrics:
- (1) Efficiency (E).
- (2) False Positive Rejection Rate (R_{fp}).
- (3) Background Alarm Rejection Rate (R_{BA}).
- d. Other:
- (1) Probability of Detection by Size and Depth.
- (2) Classification by type (i.e., 20-, 40-, 105-mm, etc.).
- (3) Location accuracy.
- (4) Equipment setup, calibration time and corresponding man-hour requirements.
- (5) Survey time and corresponding man-hour requirements.
- (6) Reacquisition/resurvey time and man-hour requirements (if any).
- (7) Downtime due to system malfunctions and maintenance requirements.

1.3 STANDARD AND NONSTANDARD INERT ORDNANCE TARGETS

The standard and nonstandard ordnance items emplaced in the test areas are listed in Table 1. Standardized targets are members of a set of specific ordnance items that have identical properties to all other items in the set (caliber, configuration, size, weight, aspect ratio, material, filler, magnetic remanence, and nomenclature). Nonstandard targets are ordnance items having properties that differ from those in the set of standardized targets.

TABLE 1. INERT ORDNANCE TARGETS

| Standard Type | Nonstandard (NS) |
|------------------------------|-------------------------|
| 20-mm Projectile M55 | 20-mm Projectile M55 |
| | 20-mm Projectile M97 |
| 40-mm Grenades M385 | 40-mm Grenades M385 |
| 40-mm Projectile MKII Bodies | 40-mm Projectile M813 |
| BDU-28 Submunition | |
| BLU-26 Submunition | |
| M42 Submunition | |
| 57-mm Projectile APC M86 | |
| 60-mm Mortar M49A3 | 60-mm Mortar (JPG) |
| | 60-mm Mortar M49 |
| 2.75-inch Rocket M230 | 2.75-inch Rocket M230 |
| | 2.75-inch Rocket XM229 |
| MK 118 ROCKEYE | |
| 81-mm Mortar M374 | 81-mm Mortar (JPG) |
| | 81-mm Mortar M374 |
| 105-mm HEAT Rounds M456 | |
| 105-mm Projectile M60 | 105-mm Projectile M60 |
| 155-mm Projectile M483A1 | 155-mm Projectile M483A |
| | 500-lb Bomb |

JPG = Jefferson Proving Ground. HEAT = high-explosive, antitank

SECTION 2. DEMONSTRATION

2.1 DEMONSTRATOR INFORMATION

2.1.1 Demonstrator Point of Contact (POC) and Address

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Address: Shaw, Inc.

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2.1.2 System Description (provided by demonstrator)

Shaw's geophysical mapping technology is an engineered combination of off-the-shelf geophysical sensors, innovative navigation technologies, a flexible/configurable deployment system, and customized data acquisition software. For this demonstration a G858 magnetometer configuration has been selected. The Shaw UXO Mapper has both hardware and software components:

2.1.2.1 <u>Hardware</u>. The system hardware consists of four integrated components: (1) G858 magnetometer sensors, (2) Shaw's composite-material cart survey system, (3) Leica TPS1100 dual laser robotic total station (RTS), and (4) Crossbow solid-state gyro. Shaw's UXO Mapper was engineered as a mapping device that can be customized to adapt to a wide range of conditions seen on UXO sites. The customizations available for survey optimization (including the number, spacing, and height of the sensors; the number of wheels (2 or 4) and wheel diameter; the forward sensor distances (relative to the wheelbase); and the handle configuration (to push, pull, or tow the system)) allow the flexibility to customize the equipment configuration to respond to local site conditions and maximize data quality.

For navigation, the Shaw UXO Mapper uses RTS technology. The Leica TSP1100 RTS is a motorized robotic total station that uses automatic target recognition to track the location of the prism and has a highly accurate distance/azimuth measurement system to produce ±5-mm +2-ppm accuracy, which translates to 0.25 inches (three dimensions) at distances of up to 1400 feet.

2.1.2.2 Software. The Shaw UXO Mapper has three software components. First, customized RTS firmware is used to track the roving prism. Developed specifically for Shaw's UXO mapping applications, this firmware allows for the rapid collection of data at a rate of up to 4 Hz and outputs solutions to the base station and rover units. The firmware enables the user to optimize prism-tracking parameters for rapid recovery of lock if obstructed by trees during a survey. Second, Shaw's data control software determines precise time synchronization between

the RTS and sensor time bases, ensuring accurate collection of all data. Third, Shaw's software for data merging accommodates various sensor navigation geometries used during data collection and provides a robust framework to spatially configure sensors relative to each other and with respect to the prism location. In addition, this software allows RTS and sensor data to be merged in either a straightforward interpolation mode (for open areas) or a hybrid switching mode that alternates to "dead reckoning" for the brief periods when the RTS is obstructed in the woods.

2.1.2.3 Shaw Cart System. This composite and fiberglass cart system deploys magnetometers, gradiometers, or electromagnetic (EM) sensors. The device has been modified to replace the standard configuration of the EM61 cart system. This adaptation is critical to the collection of high-fidelity data, as the operator has enhanced control of the sensor in terms of sensor orientation.

The RTS tracks a prism mounted on the Shaw cart system in both open and wooded conditions (fig. 1). The device tracks the prism to the centimeter level in three dimensions at a rate of up to 4 Hz. The RTS and modified deployment system allows collection of the high-density, high-fidelity data needed for improved UXO detection and discrimination. Shaw's cart system allows for the rapid collection of high-fidelity data from both magnetometer and EM sensors.



Figure 1. Shaw UXO Mapper (dual sensor G858 magnetometer).

2.1.3 <u>Data Processing Description (provided by demonstrator)</u>

Shaw's standard data processing includes data leveling, statistical data assessment, grid generation, and customized data filtering to accentuate target signatures. Shaw uses software from the sensor manufacturers, in-house software, and Geosoft's Oasis Montaj and UX-Detect Software and MATLAB to complete all tasks. Collected field data are downloaded from the data acquisition system as American Standard Code for Information Interchange (ASCII) XYZ files. Custom Shaw software is used to download the data and for initial review and generation of summary statistics as well as for conversion data formats, grid making, and analysis. All activities will be documented on the Data Processing Log. The initial steps taken in the data processing flow include:

- Initial Review of Collected Data: Validate that data fall within prescribed recording ranges; establish number of points collected, data density, and time-on/time-off.
- Statistical Analysis: Review XYZ statistics describing survey coordinates and sensor values, etc.
- Data Leveling: Adjust magnetic data on the basis of initial review and statistics, calibration data, and diurnal variations.
- Data Cataloging: Store all data in Oracle database for subsequent review and analysis.
- Data Gridding: Using Geosoft, interpolate XYZ data onto 0.25-foot grid for review by a geophysicist.
- Data Filtering: After assessment, apply data filters to enhance target signatures by reducing the effects of high-frequency or low-frequency noise sources.
- Target Detection: Initially, use Shaw's automated "region growing" techniques; next, a geophysicist visually detects targets and reviews auto-detections.
- Target Analysis: Analyze magnetic data with separate methods to define target parameters. Store all target data (raw data, processed data, and analysis parameters) within Oracle database and analyze in MATLAB via a linked database connection.
- Magnetic Analysis: Model each target with an induced dipole model where a least squares fit is made to the data. This produces estimates of target location, depth, azimuth, dip, magnetic moment, and effective diameter. Analyze dipole "misfit" surfaces to produce measure of fit quality and to identify elongate and/or compound targets.

Shaw's target detection and analysis methods for the magnetic data form the basis of our target discrimination process.

2.1.4 Data Submission Format

Data were submitted for scoring in accordance with data submission protocols outlined in the Standardized UXO Technology Demonstration Site Handbook (app E, ref 1). These submitted data are not included in the report in order to protect ground truth information.

2.1.5 <u>Demonstrator Quality Assurance (QA) and Quality Control (QC) (provided by demonstrator)</u>

Quality control (QC) for geophysical mapping is ensured through utilization of qualified staff, adherence to standard procedures, and full documentation. The following procedures and logs are used to maximize standardization, repeatability, and control of mapping activities:

- Calibration Geophysical instruments used for geophysical mapping will be field-tested daily to ensure that they are operating properly. The site geophysicist will establish standard verification procedures that will be provided in the submitted Work Plans. The function of each geophysical instrument will be checked according to the manufacturer's specifications upon daily checkout by the survey teams. The site geophysicist is responsible for the assessment of instrument functionality and will review and sign each Equipment Verification Log prior to deployment in the field.
- Data Processing Log All data from the field are run through a standard data-processing procedure. This procedure is the same for all data and is tracked with the Data Processing Log, which documents all coordinate transformations, visual data-quality checks, statistical data-quality checks, survey-coverage statistics, interpolation parameters, etc.
- Crew Deployment Log This log defines the location of each geophysical survey crew
 on a daily basis. The log tracks crewmembers, equipment, and the expected area to be
 surveyed. Attached to this daily log are maps of the areas to be surveyed containing the
 coordinates of benchmarks in the areas as well as the coordinate of each quadrant
 corner.
- Field Activity Log This log is filled out by each crew chief and details all activities of the survey. This daily log contains observations about crew performance, sensor performance, site conditions, and weather changes.
- Equipment Verification Log This log documents the daily calibration of each field instrument. Daily calibration procedures are executed for each geophysical and navigational instrument. The sensor system is brought to a calibration area before each survey day starts, and the background magnetic field and the magnetic field signal from a reference target are measured and recorded.
- Data Control Log This log is kept in the office trailer for tracking all data flowing in from the field and out of the office. Included are all geophysical field data, sensor verification data (via Equipment Verification Logs), all field notes from Field Activity Logs, and all RTS quadrant coordinate data.

- Data Analysis Log All data reduction, processing, and analysis steps are documented through this form. Each log is checked by the project geophysicist for completeness and adherence to predefined procedures.
- Target Reanalysis All targets analyzed as part of the project will be subject to review by the project geophysicist. In addition, a minimum of 10 percent of all targets will be reanalyzed by a separate geophysicist to ensure data quality.

Quality assurance (QA) measures the QC activities described above. To ensure complete and continuous area coverage, the magnetometer will collect data in 6-foot swaths. Since the magnetometer sensors are 1.5 feet apart, the effective line spacing will be 1.5 feet. Deviations from the line spacing are anticipated where obstructions such as trees exist. Maps of the traverses will be plotted and obstructions will be verified.

In addition, standardization procedures will be implemented on a site-specific basis to maximize efficiency and to adjust to logistical and schedule requirements. The procedure below shall be used at the site to define the spatial accuracy of the data and check the sample-rate selection as well as the repeatability of the sensor readings:

- a. A 50-foot-long straight-line transect will be established with the positions of the end points and midpoint logged via RTS. Wherever possible, the traverse line will be oriented north-south.
- b. Each survey system (sensor and navigation unit) used to collect data will be operated over the transect each day following these steps:
 - An operator will log "background" data along the traverse, first heading north from the southern end point, and then returning south from the northern end point.
 - A metallic target such as a trailer-hitch ball or pin flag shall be placed over the midpoint.
 - The operator will log data along the same path, first traveling north, then returning south.
 - The operator will log data along the same path, first traveling north at a slow pace, then returning south at a significantly more rapid pace.
- c. All data lines will be downloaded and provided to the site geophysicist for review. These data will be examined to determine the repeatability of the anomaly amplitude and the repeatability of the positional location of the amplitude peak.

2.1.6 Additional Records

The following record(s) by this vendor can be accessed via the Internet as MicroSoft Word documents at www.uxotestsites.org.

2.2 APG SITE INFORMATION

2.2.1 Location

The APG Standardized Test Site is located within a secured range area of the Aberdeen Area of APG. The Aberdeen Area of APG is located approximately 30 miles northeast of Baltimore at the northern end of the Chesapeake Bay. The Standardized Test Site encompasses 17 acres of upland and lowland flats, woods, and wetlands.

2.2.2 Soil Type

According to the soils survey conducted for the entire area of APG in 1998, the test site consists primarily of Elkton Series type soil (ref 2). The Elkton Series consists of very deep, slowly permeable, poorly drained soils. These soils formed in silty aeolin sediments and the underlying loamy alluvial and marine sediments. They are on upland and lowland flats and in depressions of the Mid-Atlantic Coastal Plain. Slopes range from 0 to 2 percent.

ERDC conducted a site-specific analysis in May of 2002 (ref 3). The results basically matched the soil survey mentioned above. Seventy percent of the samples taken were classified as silty loam. The majority (77 percent) of the soil samples had a measured water content between 15- and 30-percent with the water content decreasing slightly with depth.

For more details concerning the soil properties at the APG test site, go to www.uxotestsites.org on the web to view the entire soils description report.

2.2.3 Test Areas

A description of the test site areas at APG is included in Table 2.

TABLE 2. TEST SITE AREAS

| Area | Description | | | | |
|------------------|---|--|--|--|--|
| Calibration Grid | Contains 14 standard ordnance items buried in six positions at various angles and depths to allow demonstrator equipment calibration. | | | | |
| Blind Grid | Contains 400 grid cells in a 0.2-hectare (0.5 acre) site. The center of each grid cell contains ordnance, clutter or nothing. | | | | |

SECTION 3. FIELD DATA

3.1 DATE OF FIELD ACTIVITIES (19 December 2003)

3.2 AREAS TESTED/NUMBER OF HOURS

Areas tested and total number of hours operated at each site are summarized in Table 3.

TABLE 3. AREAS TESTED AND NUMBER OF HOURS

| Area | Number of Hours | | |
|-------------------|-----------------|--|--|
| Calibration Lanes | 0.00 | | |
| Blind Grid | 0.33 | | |

3.3 TEST CONDITIONS

3.3.1 Weather Conditions

An ATC weather station located approximately 2 miles west of the test site was used to record average temperature and precipitation on an hourly basis for each day of operation. The temperatures listed in Table 4 represent the average temperature during field operations from 0700 through 1700 hours while the precipitation data represents a daily total amount of rainfall. Hourly weather logs used to generate this summary are provided in Appendix B.

TABLE 4. TEMPERATURE/PRECIPITATION DATA SUMMARY

| Date, 2003 | Average Temperature, °F | Total Daily Precipitation, in. |
|-------------|-------------------------|--------------------------------|
| 19 December | 33.9 | 0.00 |

3.3.2 Field Conditions

Shaw surveyed the Blind Grid with the UXO Mapper dual sensor G858 magnetometer configuration on 19 December 2003. The Blind Grid area was muddy and frozen in areas due to rain and snow events that occurred before testing.

3.3.3 Soil Moisture

Five soil probes were placed at various locations of the site to capture soil moisture data: wet, wooded, and open areas, the calibration lanes, and blind grid/moguls. Measurements were collected in percent moisture and were taken twice daily (morning and afternoon) from five different soil layers (0 to 6 in., 6 to 12 in., 12 to 24 in., 24 to 36 in., and 36 to 48 in.) from each probe. Soil moisture logs are included in Appendix C.

3.4 FIELD ACTIVITIES

3.4.1 Setup/Mobilization

These activities included initial mobilization and daily equipment preparation and breakdown. The four-person crew took 1-hour and 25 minutes to perform the initial setup and mobilization. There was no time needed for daily equipment preparation and/or end of the day equipment breakdown. Shaw requested to run the 2 sensor configuration in the Woods area, ATC agreed to accommodate the request as long as the Blind Grid was surveyed as well.

3.4.2 Calibration

Shaw did not spend any time in the calibration lanes during this 2 sensor configuration. They did however spend 5 minutes in the Blind Grid area calibrating using a trailer hitch.

3.4.3 **Downtime Occasions**

Occasions of downtime are grouped into five categories: equipment/data checks or equipment maintenance, equipment failure and repair, weather, Demonstration Site issues, or breaks/lunch. All downtime is included for the purposes of calculating labor costs (section 5) except for downtime due to Demonstration Site issues. Demonstration Site issues, while noted in the Daily Log, are considered non-chargeable downtime for the purposes of calculating labor costs and are not discussed. Breaks and lunches are included in this section and billed to the total Site Survey area.

- **3.4.3.1** Equipment/data checks, maintenance. No equipment checks were conducted while performing this survey.
- **3.4.3.2** Equipment failure or repair. No failures occurred while surveying the Blind Grid.
- **3.4.3.3** Weather. No delays occurred due to weather.

3.4.4 Data Collection

Shaw spent a total time of 15 minutes in the Blind Grid area, all of which was spent collecting data.

3.4.5 Demobilization

The Shaw team performed a full site demonstration. Therefore, demobilization did not take place until 19 December 2003, when the crew spent 2 hours and 40 minutes packing up their equipment.

3.5 PROCESSING TIME

Shaw submitted the raw data from demonstration activities prior to leaving the site on the last day of the surveying. The scoring submission data were also provided within the required 30-day timeframe.

3.6 DEMONSTRATOR'S FIELD PERSONNEL

Lead Geophysicist:

John Dolynchuk

Project Geophysicist:

Kent Boler

Staff Geophysicist:

Jeremy Flemmer

Site Geophysicist:

Raul Fonda

3.7 DEMONSTRATOR'S FIELD SURVEYING METHOD

Shaw started surveying the blind grid in the northeast portion and surveyed in an east/west direction. One lane was surveyed and then the demonstrator returned to the beginning of the next lane (example: 1A, 1B, 1C then 2A, 2B, 2C) until completion.

3.8 SUMMARY OF DAILY LOGS

Daily logs capture all field activities during this demonstration and are located in Appendix D. Activities pertinent to this specific demonstration are indicated in highlighted text.

Shaw's UXO Mapper system can accommodate up to four sensors. The original four-sensor configuration system was used before to this demonstration to survey the Blind Grid and Open Field areas. Shaw requested to use the dual sensor configuration in the wooded area. ATC accommodated this request but required that the dual sensor configuration be used to survey the Blind Grid so that a direct comparison of the system performance could be conducted.

SECTION 4. TECHNICAL PERFORMANCE RESULTS

4.1 ROC CURVES USING ALL ORDNANCE CATEGORIES

Figure 2 shows the probability of detection for the response stage (Pd^{res}) and the discrimination stage (Pd^{disc}) versus their respective probability of false positive. Figure 3 shows both probabilities plotted against their respective probability of background alarm. Both figures use horizontal lines to illustrate the performance of the demonstrator at two demonstrator-specified points: at the system noise level for the response stage, representing the point below which targets are not considered detectable, and at the demonstrator's recommended threshold level for the discrimination stage, defining the subset of targets the demonstrator would recommend digging based on discrimination. Note that all points have been rounded to protect the ground-truth.

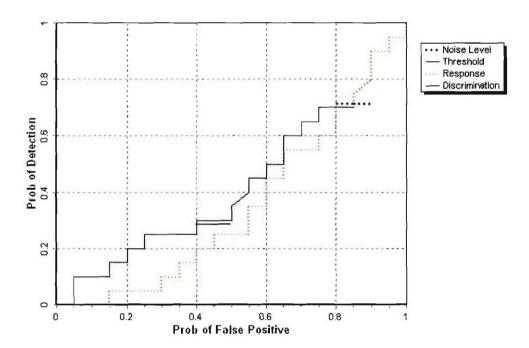


Figure 2. UXO Mapper (dual sensor magnetometer) blind grid probability of detection for response and discrimination stages versus their respective probability of false positive over all ordnance categories combined.

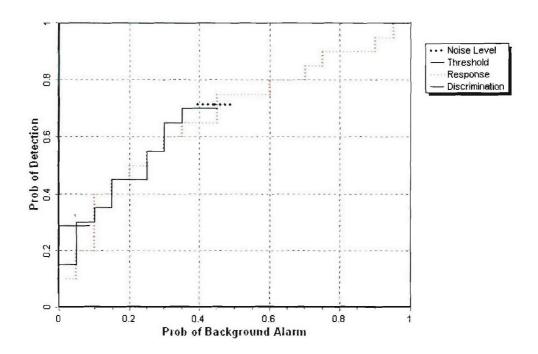


Figure 3. UXO Mapper (dual sensor magnetometer) blind grid probability of detection for response and discrimination stages versus their respective probability of background alarm over all ordnance categories combined.

4.2 ROC CURVES USING ORDNANCE LARGER THAN 20 MM

Figure 4 shows the probability of detection for the response stage (Pd^{res}) and the discrimination stage (Pd^{disc}) versus their respective probability of false positive when only targets larger than 20 mm are scored. Figure 5 shows both probabilities plotted against their respective probability of background alarm. Both figures use horizontal lines to illustrate the performance of the demonstrator at two demonstrator-specified points: at the system noise level for the response stage, representing the point below which targets are not considered detectable, and at the demonstrator's recommended threshold level for the discrimination stage, defining the subset of targets the demonstrator would recommend digging based on discrimination. Note that all points have been rounded to protect the ground truth.

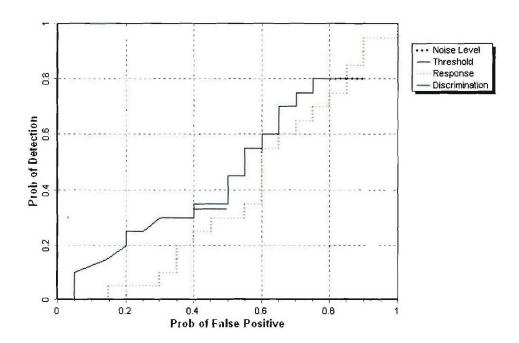


Figure 4. UXO Mapper (dual sensor magnetometer) blind grid probability of detection for response and discrimination stages versus their respective probability of false positive for all ordnance larger than 20 mm.

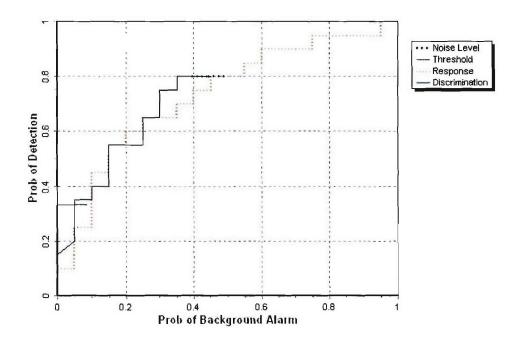


Figure 5. UXO Mapper (dual sensor magnetometer) blind grid probability of detection for response and discrimination stages versus their respective probability of background alarm for all ordnance larger than 20 mm.

4.3 PERFORMANCE SUMMARIES

Results for the Blind Grid test, broken out by size, depth and nonstandard ordnance, are presented in Tables 5a and 5b (for cost results, see section 5). Results by size and depth include both standard and nonstandard ordnance. The results by size show how well the demonstrator did at detecting/discriminating ordnance of a certain caliber range (see app A for size definitions). The results are relative to the number of ordnances emplaced. Depth is measured from the geometeric center of anomalies.

The RESPONSE STAGE results are derived from the list of anomalies above the demonstrator-provided noise level. The results for the DISCRIMINATION STAGE are derived from the demonstrator's recommended threshold for optimizing UXO field cleanup by minimizing false digs and maximizing ordnance recovery. The lower 90-percent confidence limit on probability of detection and probability of false positive was calculated assuming that the number of detections and false positives are binomially distributed random variables. All results in Tables 5a and 5b have been rounded to protect the ground truth. However, lower confidence limits were calculated using actual results.

The overall ground truth is composed of ferrous and non-ferrous anomalies. Due to limitations of the magnetometer, the non-ferrous items cannot be detected. Therefore, the summary presented in Table 5a exhibits results based on the subset of the ground truth that is solely the ferrous anomalies. Table 5b exhibits results based on the full ground truth. The response stage noise level and recommended discrimination stage threshold values are provided by the demonstrator.

TABLE 5a. SUMMARY OF BLIND GRID RESULTS (FERROUS ONLY)

| | | Standard | Nonstandard | | By Size | | | By Depth, m | | |
|--------------------------------|---------|----------|----------------|---------|---------|-------|-------|-------------|------|--|
| Metric | Overall | | | Small | Medium | Large | < 0.3 | 0.3 to <1 | >= 1 | |
| | | | RESPONSE S | STAGE | | | | | | |
| P _d | 0.70 | 0.75 | 0.70 | 0.55 | 0.80 | 0.90 | 0.65 | 0.80 | 0.70 | |
| Pd Low 90% Conf | 0.63 | 0.63 | 0.53 | 0.42 | 0.68 | 0.66 | 0.52 | 0.65 | 0.48 | |
| P _d Upper 90% Conf | 0.79 | 0.82 | 0.80 | 0.68 | 0.90 | 0.99 | 0.77 | 0.88 | 0.86 | |
| P _{fp} | 0.85 | - | - | | - | - | 0.85 | 0.85 | 1.00 | |
| Pfp Low 90% Conf | 0.79 | - | | | - | - | 0.74 | 0.76 | 0.63 | |
| P _{fp} Upper 90% Conf | 0.90 | | | - | - | - | 0.90 | 0.92 | 1.00 | |
| P _{ba} | 0.45 | | | - | - | - | - | - | - | |
| | | | DISCRIMINATION | ON STAG | E | | | | | |
| P _d | 0.30 | 0.35 | 0.20 | 0.10 | 0.40 | 0.50 | 0.30 | 0.30 | 0.25 | |
| Pd Low 90% Conf | 0.21 | 0.24 | 0.10 | 0.04 | 0.27 | 0.27 | 0.17 | 0.20 | 0.09 | |
| P _d Upper 90% Conf | 0.37 | 0.44 | 0.34 | 0.22 | 0.52 | 0.73 | 0.41 | 0.46 | 0.44 | |
| P _{fp} | 0.45 | - | | - | 7- | 7- | 0.45 | 0.45 | 0.40 | |
| P _{fp} Low 90% Conf | 0.38 | | _ | - | - | - | 0.35 | 0.35 | 0.11 | |
| P _{fp} Upper 90% Conf | 0.52 | - | ÷ | - | - | - | 0.55 | 0.56 | 0.75 | |
| P _{ba} | 0.05 | - | - | - | - | - | - | - | - | |

Response Stage Noise Level: 9.55.

Recommended Discrimination Stage Threshold: 6.95.

TABLE 5b. SUMMARY OF BLIND GRID RESULTS (FULL GROUND TRUTH)

| | | | | | By Size | | | By Depth, m | | |
|--------------------------------|---------|----------|---------------|---------|---------|-------|-------|-------------|------|--|
| Metric | Overall | Standard | Nonstandard | Small | Medium | Large | < 0.3 | 0.3 to <1 | >= 1 | |
| | | | RESPONSE S | STAGE | | | | | | |
| P_d | 0.65 | 0.70 | 0.55 | 0.45 | 0.80 | 0.90 | 0.55 | 0.75 | 0.65 | |
| P _d Low 90% Conf | 0.56 | 0.59 | 0.43 | 0.35 | 0.68 | 0.66 | 0.44 | 0.63 | 0.44 | |
| P _d Upper 90% Conf | 0.71 | 0.77 | 0.68 | 0.56 | 0.90 | 0.99 | 0.66 | 0.86 | 0.81 | |
| P _{fp} | 0.85 | - | | | | - | 0.85 | 0.85 | 1.00 | |
| P _{fp} Low 90% Conf | 0.79 | - | <u> </u> | - | | - | 0.74 | 0.76 | 0.63 | |
| P _{fp} Upper 90% Conf | 0.90 | - | | - | | - | 0.90 | 0.92 | 1.00 | |
| P _{ba} | 0.45 | - | | - | - | - | = | = | | |
| , | | | DISCRIMINATIO | ON STAG | E | | | | | |
| P _d | 0.25 | 0.30 | 0.15 | 0.05 | 0.40 | 0.50 | 0.20 | 0.30 | 0.20 | |
| Pd Low 90% Conf | 0.18 | 0.21 | 0.08 | 0.03 | 0.27 | 0.27 | 0.12 | 0.20 | 0.08 | |
| P _d Upper 90% Conf | 0.31 | 0.39 | 0.27 | 0.15 | 0.52 | 0.73 | 0.30 | 0.45 | 0.42 | |
| Pfp | 0.45 | _ | - | - | - | - | 0.45 | 0.45 | 0.40 | |
| P _{sp} Low 90% Conf | 0.38 | - | - | - | - | - | 0.35 | 0.35 | 0.11 | |
| P _{fp} Upper 90% Conf | 0.52 | - | | - | | - | 0.55 | 0.56 | 0.75 | |
| P _{ba} | 0.05 | _ | | - | - | - | - | - | - | |

Response Stage Noise Level: 9.55.

Recommended Discrimination Stage Threshold 6.95.

4.4 EFFICIENCY, REJECTION RATES, AND TYPE CLASSIFICATION

Efficiency and rejection rates are calculated to quantify the discrimination ability at specific points of interest on the ROC curve: (1) at the point where no decrease in P_d is suffered (i.e., the efficiency is by definition equal to one) and (2) at the operator selected threshold. These values are reported in Table 6.

TABLE 6. EFFICIENCY AND REJECTION RATES

| | Efficiency (E) | False Positive Rejection Rate | Background Alarm Rejection Rate |
|--------------------|----------------|----------------------------------|------------------------------------|
| At Operating Point | 0.40 | 0.48 | 0.91 |
| With No Loss of Pd | 1.00 | 0.01 | 0.11 |

At the demonstrator's recommended setting, the ordnance items that were detected and correctly discriminated were further scored on whether their correct type could be identified (table 8). Correct type examples include "20-mm projectile, 105-mm HEAT Projectile, and 2.75-inch Rocket". A list of the standard type declaration required for each ordnance item was provided to demonstrators prior to testing. For example, the standard type for the three example items are 20mmP, 105H, and 2.75in, respectively.

TABLE 7. CORRECT TYPE CLASSIFICATION OF TARGETS CORRECTLY DISCRIMINATED AS UXO

| Size | Percentage Correct | | | |
|---------|--------------------|--|--|--|
| Small | N/A | | | |
| Medium | N/A | | | |
| Large | N/A | | | |
| Overall | N/A | | | |

Note: The demonstrator did not attempt to provide type classification.

4.5 LOCATION ACCURACY

The mean location error and standard deviations appear in Table 8. These calculations are based on average missed depth for ordnance correctly identified in the discrimination stage. Depths are measured from the closest point of the ordnance to the surface. For the Blind Grid, only depth errors are calculated, since (X, Y) positions are known to be the centers of each grid square.

TABLE 8. MEAN LOCATION ERROR AND STANDARD DEVIATION (M)

| | Mean | Standard Deviation |
|-------|------|---------------------------|
| Depth | N/A | N/A |

Note: The demonstrator did not attempt to declare depth of detection.

SECTION 5. ON-SITE LABOR COSTS

A standardized estimate for labor costs associated with this effort was calculated as follows: the first person at the test site was designated "supervisor", the second person was designated "data analyst", and the third and following personnel were considered "field support". Standardized hourly labor rates were charged by title: supervisor at \$95.00/hour, data analyst at \$57.00/hour, and field support at \$28.50/hour.

Government representatives monitored on-site activity. All on-site activities were grouped into one of ten categories: initial setup/mobilization, daily setup/stop, calibration, collecting data, downtime due to break/lunch, downtime due to equipment failure, downtime due to equipment/data checks or maintenance, downtime due to weather, downtime due to demonstration site issue, or demobilization. See Appendix D for the daily activity log. See section 3.4 for a summary of field activities.

The standardized cost estimate associated with the labor needed to perform the field activities is presented in Table 9. Note that calibration time includes time spent in the Calibration Lanes as well as field calibrations. "Site survey time" includes daily setup/stop time, collecting data, breaks/lunch, downtime due to equipment/data checks or maintenance, downtime due to failure, and downtime due to weather.

TABLE 9. ON-SITE LABOR COSTS

| | No. People | Hourly Wage | Hours | Cost |
|---------------|------------|--------------|-------|----------|
| | II | NITIAL SETUP | | |
| Supervisor | 1 | \$95.00 | 1.42 | \$134.90 |
| Data Analyst | 1 | 57.00 | 1.42 | 80.94 |
| Field Support | 2 | 28.50 | 1.42 | 80.94 |
| Subtotal | | | | \$296.78 |
| | (| CALIBRATION | | |
| Supervisor | 1 | \$95.00 | 0.08 | \$7.60 |
| Data Analyst | 1 | 57.00 | 0.08 | 4.56 |
| Field Support | 2 | 28.50 | 0.08 | 4.56 |
| Subtotal | | | | \$16.72 |
| | | SITE SURVEY | | |
| Supervisor | 1 | \$95.00 | 0.25 | \$23.75 |
| Data Analyst | 1 | 57.00 | 0.25 | 14.25 |
| Field Support | 2 | 28.50 | 0.25 | 14.25 |
| Subtotal | | | | \$52.25 |

See notes at end of table.

TABLE 9 (CONT'D)

| | No. People | Hourly Wage | Hours | Cost |
|---------------|------------|--------------|-------|----------|
| | DE | MOBILIZATION | | |
| Supervisor | 1 | \$95.00 | 2.67 | \$253.65 |
| Data Analyst | 1 | 57.00 | 2.67 | 152.19 |
| Field Support | 2 | 28.50 | 2.67 | 152.19 |
| Subtotal | | | | \$558.03 |
| Total | | | | \$923.78 |

Notes: Calibration time includes time spent in the Calibration Lanes as well as calibration before each data run.

Site Survey time includes daily setup/stop time, collecting data, breaks/lunch, downtime due to system maintenance, failure, and weather.

SECTION 6. COMPARISON OF RESULTS TO DATE

No comparisons to date.

3

SECTION 7. APPENDIXES

APPENDIX A. TERMS AND DEFINITIONS

GENERAL DEFINITIONS

Anomaly: Location of a system response deemed to warrant further investigation by the demonstrator for consideration as an emplaced ordnance item.

Detection: An anomaly location that is within R_{halo} of an emplaced ordnance item.

Emplaced Ordnance: An ordnance item buried by the government at a specified location in the test site.

Emplaced Clutter: A clutter item (i.e., non-ordnance item) buried by the government at a specified location in the test site.

 R_{halo} : A predetermined radius about the periphery of an emplaced item (clutter or ordnance) within which a location identified by the demonstrator as being of interest is considered to be a response from that item. If multiple declarations lie within R_{halo} of any item (clutter or ordnance), the declaration with the highest signal output within the R_{halo} will be utilized. For the purpose of this program, a circular halo 0.5 meter in radius will be placed around the center of the object for all clutter and ordnance items less than 0.6 meter in length. When ordnance items are longer than 0.6 meter, the halo becomes an ellipse where the minor axis remains 1 meter and the major axis is equal to the length of the ordnance plus 1 meter.

Small Ordnance: Caliber of ordnance less than or equal to 40 mm (includes 20-mm projectile, 40-mm projectile, submunitions BLU-26, BLU-63, and M42).

Medium Ordnance: Caliber of ordnance greater than 40 mm and less than or equal to 81 mm (includes 57-mm projectile, 60-mm mortar, 2.75 inch Rocket, MK118 Rockeye, 81-mm mortar).

Large Ordnance: Caliber of ordnance greater than 81-mm (includes 105-mm HEAT, 105-mm projectile, 155-mm projectile, 500-lb bomb).

Shallow: Items buried less than 0.3 meter below ground surface.

Medium: Items buried greater than or equal to 0.3 meter and less than 1 meter below ground surface.

Deep: Items buried greater than or equal to 1 meter below ground surface.

Response Stage Noise Level: The level that represents the point below which anomalies are not considered detectable. Demonstrators are required to provide the recommended noise level for the Blind Grid test area.

Discrimination Stage Threshold: The demonstrator selected threshold level that they believe provides optimum performance of the system by retaining all detectable ordnance and rejecting the maximum amount of clutter. This level defines the subset of anomalies the demonstrator would recommend digging based on discrimination.

Binomially Distributed Random Variable: A random variable of the type which has only two possible outcomes, say success and failure, is repeated for n independent trials with the probability p of success and the probability 1-p of failure being the same for each trial. The number of successes x observed in the n trials is an estimate of p and is considered to be a binomially distributed random variable.

RESPONSE AND DISCRIMINATION STAGE DATA

The scoring of the demonstrator's performance is conducted in two stages. These two stages are termed the RESPONSE STAGE and DISCRIMINATION STAGE. For both stages, the probability of detection (P_d) and the false alarms are reported as receiver-operating characteristic (ROC) curves. False alarms are divided into those anomalies that correspond to emplaced clutter items, measuring the probability of false positive (P_{fp}) and those that do not correspond to any known item, termed background alarms.

The RESPONSE STAGE scoring evaluates the ability of the system to detect emplaced targets without regard to ability to discriminate ordnance from other anomalies. For the RESPONSE STAGE, the demonstrator provides the scoring committee with the location and signal strength of all anomalies that the demonstrator has deemed sufficient to warrant further investigation and/or processing as potential emplaced ordnance items. This list is generated with minimal processing (e.g., this list will include all signals above the system noise threshold). As such, it represents the most inclusive list of anomalies.

The DISCRIMINATION STAGE evaluates the demonstrator's ability to correctly identify ordnance as such, and to reject clutter. For the same locations as in the RESPONSE STAGE anomaly list, the DISCRIMINATION STAGE list contains the output of the algorithms applied in the discrimination-stage processing. This list is prioritized based on the demonstrator's determination that an anomaly location is likely to contain ordnance. Thus, higher output values are indicative of higher confidence that an ordnance item is present at the specified location. For electronic signal processing, priority ranking is based on algorithm output. For other systems, priority ranking is based on human judgment. The demonstrator also selects the threshold that the demonstrator believes will provide "optimum" system performance, (i.e., that retains all the detected ordnance and rejects the maximum amount of clutter).

Note: The two lists provided by the demonstrator contain identical numbers of potential target locations. They differ only in the priority ranking of the declarations.

RESPONSE STAGE DEFINITIONS

Response Stage Probability of Detection (P_d^{res}) : $P_d^{res} = (No. of response-stage detections)/(No. of emplaced ordnance in the test site).$

Response Stage False Positive (fp^{res}): An anomaly location that is within R_{halo} of an emplaced clutter item.

Response Stage Probability of False Positive (P_{fp}^{res}) : $P_{fp}^{res} = (No. of response-stage false positives)/(No. of emplaced clutter items).$

Response Stage Background Alarm (ba^{res}): An anomaly in a blind grid cell that contains neither emplaced ordnance nor an emplaced clutter item. An anomaly location in the open field or scenarios that is outside R_{halo} of any emplaced ordnance or emplaced clutter item.

Response Stage Probability of Background Alarm (P_{ba}^{res}): Blind Grid only: $P_{ba}^{res} = (No. of response-stage background alarms)/(No. of empty grid locations).$

Response Stage Background Alarm Rate (BAR^{res}): Open Field only: BAR^{res} = (No. of response-stage background alarms)/(arbitrary constant).

Note that the quantities P_d^{res} , P_{fp}^{res} , P_{ba}^{res} , and BAR^{res} are functions of t^{res} , the threshold applied to the response-stage signal strength. These quantities can therefore be written as $P_d^{res}(t^{res})$, $P_{fp}^{res}(t^{res})$, $P_{ba}^{res}(t^{res})$, and $BAR^{res}(t^{res})$.

DISCRIMINATION STAGE DEFINITIONS

Discrimination: The application of a signal processing algorithm or human judgment to response-stage data that discriminates ordnance from clutter. Discrimination should identify anomalies that the demonstrator has high confidence correspond to ordnance, as well as those that the demonstrator has high confidence correspond to non-ordnance or background returns. The former should be ranked with highest priority and the latter with lowest.

Discrimination Stage Probability of Detection (P_d^{disc}) : $P_d^{disc} = (No. of discrimination-stage detections)/(No. of emplaced ordnance in the test site).$

Discrimination Stage False Positive (fp^{disc}): An anomaly location that is within R_{halo} of an emplaced clutter item.

Discrimination Stage Probability of False Positive (P_{fp}^{disc}): $P_{fp}^{disc} = (No. of discrimination stage false positives)/(No. of emplaced clutter items).$

Discrimination Stage Background Alarm (ba^{disc}): An anomaly in a blind grid cell that contains neither emplaced ordnance nor an emplaced clutter item. An anomaly location in the open field or scenarios that is outside R_{halo} of any emplaced ordnance or emplaced clutter item.

Discrimination Stage Probability of Background Alarm (P_{ba}^{disc}): P_{ba}^{disc} = (No. of discrimination-stage background alarms)/(No. of empty grid locations).

Discrimination Stage Background Alarm Rate (BAR^{disc}): BAR^{disc} = (No. of discrimination-stage background alarms)/(arbitrary constant).

Note that the quantities P_d^{disc} , P_{fp}^{disc} , P_{ba}^{disc} , and BAR^{disc} are functions of t^{disc} , the threshold applied to the discrimination-stage signal strength. These quantities can therefore be written as $P_d^{disc}(t^{disc})$, $P_{fp}^{disc}(t^{disc})$, $P_{ba}^{disc}(t^{disc})$, and $BAR^{disc}(t^{disc})$.

RECEIVER-OPERATING CHARACERISTIC (ROC) CURVES

ROC curves at both the response and discrimination stages can be constructed based on the above definitions. The ROC curves plot the relationship between P_d versus P_{fp} and P_d versus BAR or P_{ba} as the threshold applied to the signal strength is varied from its minimum (t_{min}) to its maximum (t_{max}) value. Figure A-1 shows how P_d versus P_{fp} and P_d versus BAR are combined into ROC curves. Note that the "res" and "disc" superscripts have been suppressed from all the variables for clarity.

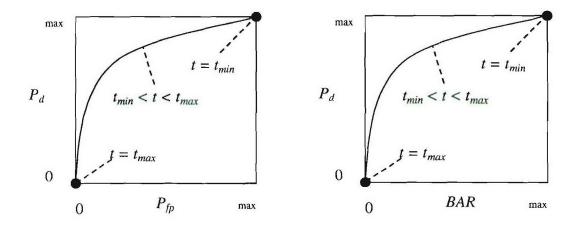


Figure A-1. ROC curves for open-field testing. Each curve applies to both the response and discrimination stages.

Strictly speaking, ROC curves plot the P_d versus P_{ba} over a predetermined and fixed number of detection opportunities (some of the opportunities are located over ordnance and others are located over clutter or blank spots). In an Open Field scenario, each system suppresses its signal strength reports until some bare-minimum signal response is received by the system. Consequently, the open field ROC curves do not have information from low signal-output locations, and, furthermore, different contractors report their signals over a different set of locations on the ground. These ROC curves are thus not true to the strict definition of ROC curves as defined in textbooks on detection theory. Note, however, that the ROC curves obtained in the Blind Grid test sites are true ROC curves.

METRICS TO CHARACTERIZE THE DISCRIMINATION STAGE

The demonstrator is also scored on efficiency and rejection ratio, which measure the effectiveness of the discrimination stage processing. The goal of discrimination is to retain the greatest number of ordnance detections from the anomaly list, while rejecting the maximum number of anomalies arising from non-ordnance items. The efficiency measures the amount of detected ordnance retained by the discrimination, while the rejection ratio measures the fraction of false alarms rejected. Both measures are defined relative to the entire response list, i.e., the maximum ordnance detectable by the sensor and its accompanying false positive rate or background alarm rate.

Efficiency (E): $E = P_d^{disc}(t^{disc})/P_d^{res}(t_{min}^{res})$ Measures (at a threshold of interest), the degree to which the maximum theoretical detection performance of the sensor system (as determined by the response stage tmin) is preserved after application of discrimination techniques. Efficiency is a number between 0 and 1. An efficiency of 1 implies that all of the ordnance initially detected in the response stage was retained at the specified threshold in the discrimination stage, t^{disc} .

False-Positive Rejection Rate (R_{fp}): $R_{fp} = 1 - [P_{fp}^{\ disc}(t^{\ disc})/P_{fp}^{\ res}(t_{min}^{\ res})]$; Measures (at a threshold of interest), the degree to which the sensor system's false positive performance is improved over the maximum false positive performance (as determined by the response stage t_{min}). The rejection rate is a number between 0 and 1. A rejection rate of 1 implies that all emplaced clutter initially detected in the response stage were correctly rejected at the specified threshold in the discrimination stage.

Background Alarm Rejection Rate (Rba):

```
Blind Grid: R_{ba} = 1 - [P_{ba}^{disc}(t^{disc})/P_{ba}^{res}(t_{min}^{res})]
Open Field: R_{ba} = 1 - [BAR^{disc}(t^{disc})/BAR^{res}(t_{min}^{res})])
```

Measures the degree to which the discrimination stage correctly rejects background alarms initially detected in the response stage. The rejection rate is a number between 0 and 1. A rejection rate of 1 implies that all background alarms initially detected in the response stage were rejected at the specified threshold in the discrimination stage.

CHI-SQUARE COMPARISON EXPLANATION:

The Chi-square test for differences in probabilities (or 2 x 2 contingency table) is used to analyze two samples drawn from two different populations to see if both populations have the same or different proportions of elements in a certain category. More specifically, two random samples are drawn, one from each population, to test the null hypothesis that the probability of event A (some specified event) is the same for both populations (ref 4).

A 2 x 2 contingency table is used in the Standardized UXO Technology Demonstration Site Program to determine if there is reason to believe that the proportion of ordnance correctly detected/discriminated by demonstrator X's system is significantly degraded by the more

challenging terrain feature introduced. The test statistic of the 2 x 2 contingency table is the Chi-square distribution with one degree of freedom. Since an association between the more challenging terrain feature and relatively degraded performance is sought, a one-sided test is performed. A significance level of 0.05 is chosen which sets a critical decision limit of 2.71 from the Chi-square distribution with one degree of freedom. It is a critical decision limit because if the test statistic calculated from the data exceeds this value, the two proportions tested will be considered significantly different. If the test statistic calculated from the data is less than this value, the two proportions tested will be considered not significantly different.

An exception must be applied when either a 0 or 100 percent success rate occurs in the sample data. The Chi-square test cannot be used in these instances. Instead, Fischer's test is used and the critical decision limit for one-sided tests is the chosen significance level, which in this case is 0.05. With Fischer's test, if the test statistic is less than the critical value, the proportions are considered to be significantly different.

Standardized UXO Technology Demonstration Site examples, where blind grid results are compared to those from the open field and open field results are compared to those from one of the scenarios, follow. It should be noted that a significant result does not prove a cause and effect relationship exists between the two populations of interest; however, it does serve as a tool to indicate that one data set has experienced a degradation in system performance at a large enough level than can be accounted for merely by chance or random variation. Note also that a result that is not significant indicates that there is not enough evidence to declare that anything more than chance or random variation within the same population is at work between the two data sets being compared.

Demonstrator X achieves the following overall results after surveying each of the three progressively more difficult areas using the same system (results indicate the number of ordnance detected divided by the number of ordnance emplaced):

| Blind Grid | Open Field | Moguls |
|----------------------------------|------------|-------------|
| $P_d^{\text{res}} 100/100 = 1.0$ | 8/10 = .80 | 20/33 = .61 |
| $P_d^{disc} 80/100 = 0.80$ | 6/10 = .60 | 8/33 = .24 |

P_d^{res}: BLIND GRID versus OPEN FIELD. Using the example data above to compare probabilities of detection in the response stage, all 100 ordnance out of 100 emplaced ordnance items were detected in the blind grid while 8 ordnance out of 10 emplaced were detected in the open field. Fischer's test must be used since a 100 percent success rate occurs in the data. Fischer's test uses the four input values to calculate a test statistic of 0.0075 that is compared against the critical value of 0.05. Since the test statistic is less than the critical value, the smaller response stage detection rate (0.80) is considered to be significantly less at the 0.05 level of significance. While a significant result does not prove a cause and effect relationship exists between the change in survey area and degradation in performance, it does indicate that the detection ability of demonstrator X's system seems to have been degraded in the open field relative to results from the blind grid using the same system.

- P_d disc: BLIND GRID versus OPEN FIELD. Using the example data above to compare probabilities of detection in the discrimination stage, 80 out of 100 emplaced ordnance items were correctly discriminated as ordnance in blind grid testing while 6 ordnance out of 10 emplaced were correctly discriminated as such in open field testing. Those four values are used to calculate a test statistic of 1.12. Since the test statistic is less than the critical value of 2.71, the two discrimination stage detection rates are considered to be not significantly different at the 0.05 level of significance.
- P_d^{res}: OPEN FIELD versus MOGULS. Using the example data above to compare probabilities of detection in the response stage, 8 out of 10 and 20 out of 33 are used to calculate a test statistic of 0.56. Since the test statistic is less than the critical value of 2.71, the two response stage detection rates are considered to be not significantly different at the 0.05 level of significance.
- P_d^{disc} : OPEN FIELD versus MOGULS. Using the example data above to compare probabilities of detection in the discrimination stage, 6 out of 10 and 8 out of 33 are used to calculate a test statistic of 2.98. Since the test statistic is greater than the critical value of 2.71, the smaller discrimination stage detection rate is considered to be significantly less at the 0.05 level of significance. While a significant result does not prove a cause and effect relationship exists between the change in survey area and degradation in performance, it does indicate that the ability of demonstrator X to correctly discriminate seems to have been degraded by the mogul terrain relative to results from the flat open field using the same system.

APPENDIX B. DAILY WEATHER LOGS

TABLE B-1. WEATHER LOG

| Date | Time | Average Temperature, °F | Maximum Temperature, °F | Minimum Temperature, °F | RH, | Total Precipitation, in. |
|--|-------|-------------------------------|-------------------------------|-------------------------------|-------|--------------------------------|
| | 00:00 | 25.5 | 26.6 | 23.4 | 67.98 | 0.00 |
| 12/08/2003 | | 24.1 | 25.8 | 19.8 | 68.56 | 0.00 |
| 12/08/2003 | | 22.2 | 25.3 | 18.9 | 69.82 | 0.00 |
| | 03:00 | 22.2 | 23.4 | 19.5 | 69.89 | 0.00 |
| 12/08/2003 | | 22.7 | 24.0 | 20.6 | 69.22 | 0.00 |
| 12/08/2003 | - | 21.8 | 22.5 | 20.6 | 74.53 | 0.00 |
| angular and known plays and an | 06:00 | 18.4 | 21.6 | 16.1 | 83.00 | 0.00 |
| | 07:00 | 19.9 | 21.9 | 18.4 | 80.10 | 0.00 |
| 12/08/2003 | | 20.0 | 22.5 | 17.3 | 82.70 | 0.00 |
| 12/08/2003 | | 22.7 | 25.6 | 20.8 | 77.17 | 0.00 |
| | 10:00 | 29.3 | 32.9 | 24.6 | 63.19 | 0.00 |
| | 11:00 | 33.4 | 34.8 | 32.3 | 51.95 | 0.00 |
| 12/08/2003 | | 35.2 | 35.8 | 34.3 | 48.01 | 0.00 |
| 12/08/2003 | | 36.6 | 37.6 | 35.4 | 46.40 | 0.00 |
| 12/08/2003 | | 37.8 | 38.7 | 37.1 | 44.89 | 0.00 |
| | 15:00 | 38.2 | 38.7 | 37.7 | 42.75 | 0.00 |
| | 16:00 | 38.1 | 38.7 | 37.1 | 42.23 | 0.00 |
| 12/08/2003 | | 36.9 | 37.5 | 36.2 | 46.32 | 0.00 |
| | 18:00 | 35.9 | 36.5 | 35.2 | 49.55 | 0.00 |
| 12/08/2003 | | 34.5 | 35.5 | 32.0 | 52.73 | 0.00 |
| 12/08/2003 | - | 31.3 | 32.2 | 30.6 | 69.34 | 0.00 |
| 12/08/2003 | | 31.5 | 32.3 | 30.8 | 67.20 | 0.00 |
| | 22:00 | 30.0 | 31.4 | 28.7 | 72.94 | 0.00 |
| | 23:00 | 28.6 | 29.9 | 27.2 | 79.13 | 0.00 |
| 12/09/2003 | | 27.1 | 28.4 | 26.0 | 82.90 | 0.00 |
| | 01:00 | 26.0 | 26.6 | 25.3 | 84.80 | 0.00 |
| 12/09/2003 | | 25.0 | 25.9 | 24.4 | 86.20 | 0.00 |
| | 03:00 | 25.6 | 26.4 | 25.1 | 86.70 | 0.00 |
| | 04:00 | 24.5 | 26.0 | 23.3 | 86.90 | 0.00 |
| | 05:00 | 23.0 | 24.2 | 21.4 | 90.60 | 0.00 |
| A CONTRACTOR OF THE PROPERTY O | 06:00 | 22.4 | 23.5 | 21.2 | 94.90 | 0.00 |
| 12/09/2003 | 07:00 | 24.1 | 25.3 | 22.7 | 93.00 | 0.00 |
| 12/09/2003 | 08:00 | 25.5 | 26.8 | 25.0 | 91.80 | 0.00 |
| 12/09/2003 | | 28.9 | 31.6 | 26.4 | 86.60 | 0.00 |
| 12/09/2003 | - | 32.3 | 34.3 | 30.5 | 76.66 | 0.00 |
| 12/09/2003 | | 34.5 | 35.6 | 33.8 | 70.21 | 0.00 |
| 12/09/2003 | | 35.7 | 36.9 | 35.0 | 65.98 | 0.00 |
| 12/09/2003 | - | 37.9 | 38.8 | 36.7 | 60.19 | 0.02 |
| 12/09/2003 | | 37.9 | 38.8 | 37.1 | 60.14 | 0.05 |
| 12/09/2003 | | 38.4 | 39.3 | 38.0 | 57.57 | 0.02 |
| 12/09/2003 | | 38.4 | 39.3 | 37.4 | 56.83 | 0.01 |
| 12/09/2003 | | 36.9 | 37.6 | 36.1 | 64.81 | 0.00 |

TABLE B-1 (CONT'D)

| Date | Time | Average Temperature, °F | Maximum Temperature, °F | Minimum Temperature, °F | RH, | Total Precipitation, in. |
|------------|---|-------------------------------|-------------------------------|-------------------------------|--------|--------------------------------|
| 12/09/2003 | 18:00 | 36.8 | 37.3 | 36.2 | 70.68 | 0.00 |
| 12/09/2003 | 19:00 | 37.1 | 37.6 | 36.4 | 74.73 | 0.00 |
| 12/09/2003 | | 37.0 | 37.3 | 36.6 | 76.81 | 0.01 |
| 12/09/2003 | 21:00 | 36.9 | 37.4 | 36.3 | 73.92 | 0.00 |
| 12/09/2003 | or 1000-100-00-00-00-00-00-00-00-00-00-00-0 | 37.0 | 37.4 | 36.4 | 73.60 | 0.00 |
| 12/09/2003 | 23:00 | 36.8 | 37.4 | 36.3 | 78.46 | 0.01 |
| 12/10/2003 | 00:00 | 36.6 | 37.0 | 36.2 | 79.93 | 0.00 |
| 12/10/2003 | 01:00 | 36.0 | 36.8 | 35.4 | 80.80 | 0.00 |
| 12/10/2003 | 02:00 | 35.0 | 36.1 | 34.4 | 84.80 | 0.00 |
| 12/10/2003 | | 35.2 | 35.7 | 34.4 | 86.80 | 0.00 |
| 12/10/2003 | | 34.7 | 35.2 | 34.2 | 86.90 | 0.00 |
| 12/10/2003 | | 34.8 | 35.2 | 34.3 | 85.40 | 0.00 |
| 12/10/2003 | | 34.2 | 34.8 | 33.7 | 85.20 | 0.00 |
| 12/10/2003 | | 34.0 | 34.4 | 33.3 | 87.60 | 0.00 |
| 12/10/2003 | | 34.0 | 35.3 | 33.3 | 90.30 | 0.00 |
| 12/10/2003 | 09:00 | 36.2 | 38.0 | 34.7 | 86.90 | 0.00 |
| 12/10/2003 | | 38.6 | 39.3 | 37.5 | 85.20 | 0.01 |
| 12/10/2003 | | 39.6 | 40.7 | 38.4 | 85.60 | 0.01 |
| 12/10/2003 | 12:00 | 42.0 | 42.8 | 40.5 | 83.10 | 0.01 |
| 12/10/2003 | | 42.7 | 43.2 | 41.8 | 85.40 | 0.00 |
| 12/10/2003 | 14:00 | 43.1 | 43.7 | 42.5 | 87.10 | 0.01 |
| 12/10/2003 | 15:00 | 42.5 | 43.2 | 41.8 | 95.10 | 0.06 |
| 12/10/2003 | 16:00 | 42.1 | 42.9 | 41.6 | 98.10 | 0.1 |
| 12/10/2003 | 17:00 | 43.0 | 43.9 | 41.9 | 99.30 | 0.13 |
| 12/10/2003 | 18:00 | 45.9 | 48.3 | 43.0 | 99.60 | 0.02 |
| 12/10/2003 | 19:00 | 48.3 | 49.1 | 47.2 | 99.70 | 0.00 |
| 12/10/2003 | 20:00 | 48.4 | 51.7 | 47.3 | 99.80 | 0.00 |
| 12/10/2003 | 21:00 | 53.3 | 54.6 | 51.4 | 100.00 | 0.00 |
| 12/10/2003 | 22:00 | 52.8 | 53.8 | 52.1 | 99.70 | 0.00 |
| 12/10/2003 | 23:00 | 53.4 | 54.5 | 52.4 | 97.90 | 0.04 |
| 12/11/2003 | 00:00 | 53.5 | 54.6 | 52.4 | 96.20 | 0.02 |
| 12/11/2003 | 01:00 | 52.8 | 53.2 | 52.2 | 95.60 | 0.03 |
| 12/11/2003 | 02:00 | 52.7 | 53.4 | 51.5 | 96.60 | 0.05 |
| 12/11/2003 | 03:00 | 53.8 | 54.5 | 52.9 | 97.60 | 0.24 |
| 12/11/2003 | 04:00 | 55.8 | 56.8 | 53.8 | 96.20 | 0.12 |
| 12/11/2003 | - | 56.2 | 56.6 | 55.7 | 95.00 | 0.01 |
| 12/11/2003 | 06:00 | 56.7 | 57.5 | 56.0 | 96.60 | 0.02 |
| 12/11/2003 | | 57.2 | 57.9 | 55.9 | 97.90 | 0.08 |
| 12/11/2003 | | 54.2 | 56.4 | 52.3 | 92.80 | 0.00 |
| 12/11/2003 | | 51.6 | 52.8 | 50.9 | 85.40 | 0.00 |
| 12/11/2003 | | 51.6 | 52.4 | 51.1 | 81.30 | 0.00 |
| 12/11/2003 | | 52.5 | 53.3 | 52.0 | 76.59 | 0.00 |
| 12/11/2003 | | 53.1 | 53.6 | 52.4 | 71.52 | 0.00 |
| 12/11/2003 | | 52.3 | 52.9 | 51.7 | 68.36 | 0.00 |
| 12/11/2003 | 14:00 | 53.4 | 54.4 | 52.2 | 62.99 | 0.00 |

TABLE B-1 (CONT'D)

| Data | T: 0 | Average Temperature, °F | Maximum Temperature, °F | Minimum Temperature, °F | RH, | Total Precipitation, |
|-----------------|-----------------------------|-------------------------------|-------------------------------|-------------------------------|-------|-------------------------|
| Date 12/11/2003 | Time 15:00 | 52.1 | 53.9 | 50.9 | 61.83 | 0.00 |
| 12/11/2003 | | 50.5 | 51.2 | 49.7 | 62.27 | 0.00 |
| 12/11/2003 | | 47.6 | 50.0 | 45.6 | 59.74 | 0.00 |
| 12/11/2003 | 18:00 | 44.5 | 46.0 | 43.4 | 58.79 | 0.00 |
| 12/11/2003 | 200 000 000 000 | 42.7 | 43.6 | 41.8 | 57.39 | 0.00 |
| 12/11/2003 | | 41.8 | 42.7 | 41.2 | 58.06 | 0.00 |
| 12/11/2003 | | 41.1 | 41.7 | 40.4 | 59.86 | 0.00 |
| 12/11/2003 | | 40.6 | 41.1 | 39.8 | 59.69 | 0.00 |
| 12/11/2003 | | 40.1 | 40.5 | 39.5 | 58.23 | 0.00 |
| 12/12/2003 | | 39.3 | 39.9 | 38.6 | 57.36 | 0.00 |
| 12/12/2003 | 01:00 | 38.0 | 39.1 | 37.2 | 60.63 | 0.00 |
| 12/12/2003 | | 37.5 | 38.0 | 37.0 | 61.25 | 0.00 |
| 12/12/2003 | | 37.2 | 37.9 | 36.8 | 60.55 | 0.00 |
| 12/12/2003 | | 36.8 | 37.3 | 36.3 | 60.49 | 0.00 |
| 12/12/2003 | | 36.2 | 36.8 | 35.5 | 61.19 | 0.00 |
| 12/12/2003 | 06:00 | 35.8 | 36.3 | 35.5 | 61.66 | 0.00 |
| 12/12/2003 | | 35.5 | 36.1 | 35.0 | 60.61 | 0.00 |
| 12/12/2003 | | 35.4 | 36.2 | 34.8 | 59.84 | 0.00 |
| 12/12/2003 | | 37.0 | 38.1 | 35.8 | 56.70 | 0.00 |
| 12/12/2003 | Commence of the commence of | 38.5 | 39.1 | 37.6 | 50.70 | 0.00 |
| 12/12/2003 | | 39.8 | 41.3 | 38.6 | 48.92 | 0.00 |
| 12/12/2003 | | 40.7 | 41.3 | 40.0 | 47.40 | 0.00 |
| 12/12/2003 | | 41.4 | 42.2 | 40.5 | 46.41 | 0.00 |
| 12/12/2003 | | 42.3 | 42.9 | 41.6 | 44.78 | 0.00 |
| 12/12/2003 | 100 | 41.7 | 42.9 | 40.8 | 44.55 | 0.00 |
| 12/12/2003 | | 41.3 | 42.3 | 40.2 | 47.05 | 0.00 |
| 12/12/2003 | | 39.0 | 40.6 | 37.3 | 50.49 | 0.00 |
| 12/12/2003 | | 36.9 | 37.6 | 36.2 | 54.02 | 0.00 |
| 12/12/2003 | | 36.1 | 36.8 | 35.2 | 52.59 | 0.00 |
| 12/12/2003 | | 35.0 | 35.5 | 34.4 | 54.16 | 0.00 |
| 12/12/2003 | | 34.0 | 34.8 | 33.3 | 53.91 | 0.00 |
| 12/12/2003 | | 32.6 | 33.7 | 31.7 | 56.92 | 0.00 |
| 12/12/2003 | | 32.0 | 32.4 | 31.5 | 57.69 | 0.00 |
| 12/13/2003 | | 31.4 | 31.8 | 30.8 | 59.22 | 0.00 |
| 12/13/2003 | | 30.5 | 31.7 | 29.6 | 61.08 | 0.00 |
| 12/13/2003 | | 30.4 | 31.0 | 29.6 | 57.84 | 0.00 |
| 12/13/2003 | | 29.4 | 30.5 | 28.2 | 60.37 | 0.00 |
| 12/13/2003 | | 28.0 | 29.0 | 27.5 | 65.52 | 0.00 |
| 12/13/2003 | | 27.8 | 28.6 | 27.1 | 63.01 | 0.00 |
| 12/13/2003 | | 28.8 | 29.5 | 27.6 | 57.42 | 0.00 |
| 12/13/2003 | | 28.5 | 29.0 | 27.8 | 56.65 | 0.00 |
| 12/13/2003 | | 28.3 | 29.4 | 27.6 | 56.65 | 0.00 |
| 12/13/2003 | - | 29.6 | 31.0 | 28.7 | 54.93 | 0.00 |
| 12/13/2003 | | 31.8 | 32.6 | 30.6 | 51.47 | 0.00 |
| 12/13/2003 | | 33.2 | 34.6 | 32.0 | 47.89 | 0.00 |

TABLE B-1 (CONT'D)

| Date | Time | Average Temperature, °F | Maximum Temperature, °F | Minimum Temperature, °F | RH, | Total Precipitation, in. |
|--|-------|-------------------------------|-------------------------------|-------------------------------|--------|--------------------------------|
| 12/13/2003 | 12:00 | 34.5 | 35.5 | 33.3 | 43.81 | 0.00 |
| 12/13/2003 | 13:00 | 34.8 | 36.0 | 34.0 | 41.60 | 0.00 |
| 12/13/2003 | 14:00 | 35.4 | 36.2 | 34.6 | 41.27 | 0.00 |
| 12/13/2003 | 15:00 | 34.5 | 35.6 | 33.9 | 43.80 | 0.00 |
| AND THE RESIDENCE AND THE PARTY OF THE PARTY | 16:00 | 34.1 | 34.5 | 33.7 | 45.53 | 0.00 |
| | 17:00 | 33.3 | 33.9 | 32.6 | 48.90 | 0.00 |
| | 18:00 | 32.9 | 33.3 | 32.5 | 50.74 | 0.00 |
| 12/13/2003 | 19:00 | 32.9 | 33.2 | 32.6 | 51.91 | 0.00 |
| | 20:00 | 32.7 | 33.0 | 32.4 | 53.17 | 0.00 |
| | 21:00 | 32.8 | 33.1 | 32.5 | 54.07 | 0.00 |
| | 22:00 | 33.4 | 33.9 | 32.7 | 54.07 | 0.00 |
| | 23:00 | 33.7 | 33.9 | 33.3 | 52.35 | 0.00 |
| | 00:00 | 33.6 | 33.9 | 32.8 | 51.54 | 0.00 |
| | 01:00 | 32.9 | 33.4 | 32.5 | 51.63 | 0.00 |
| The second secon | 02:00 | 33.1 | 33.7 | 32.6 | 50.62 | 0.00 |
| | 03:00 | 33.5 | 33.9 | 33.1 | 52.20 | 0.00 |
| | 04:00 | 33.8 | 34.2 | 33.3 | 53.68 | 0.00 |
| 12/14/2003 | 05:00 | 34.0 | 34.3 | 33.8 | 59.10 | 0.00 |
| 12/14/2003 | | 33.5 | 34.3 | 31.8 | 70.21 | 0.00 |
| | 07:00 | 31.4 | 32.2 | 30.9 | 93.10 | 0.00 |
| 2 2 2 | 08:00 | 31.5 | 32.2 | 30.9 | 98.90 | 0.00 |
| COLD DO NOT DOOR TO DO NOT DOOR | 09:00 | 32.3 | 33.1 | 31.6 | 99.90 | 0.00 |
| 12/14/2003 | | 33.5 | 34.4 | 32.8 | 100.00 | 0.00 |
| | 11:00 | 34.4 | 34.6 | 34.0 | 98.90 | 0.13 |
| | 12:00 | 35.0 | 35.5 | 34.4 | 98.50 | 0.18 |
| | 13:00 | 35.1 | 35.7 | 34.5 | 98.30 | 0.04 |
| | 14:00 | 35.9 | 36.7 | 35.4 | 98.80 | 0.09 |
| | 15:00 | 37.3 | 38.0 | 36.3 | 99.30 | 0.06 |
| | 16:00 | 38.9 | 40.0 | 37.6 | 99.40 | 0.09 |
| 12/14/2003 | 17:00 | 40.3 | 40.9 | 39.8 | 98.90 | 0.02 |
| | 18:00 | 41.2 | 42.2 | 40.5 | 97.70 | 0.01 |
| 12/14/2003 | 19:00 | 40.8 | 42.2 | 38.6 | 97.80 | 0.07 |
| 12/14/2003 | 20:00 | 37.2 | 38.8 | 36.3 | 96.60 | 0.01 |
| 12/14/2003 | 21:00 | 36.3 | 36.7 | 35.8 | 94.00 | 0.00 |
| 12/14/2003 | 22:00 | 36.0 | 36.4 | 35.7 | 93.80 | 0.00 |
| 12/14/2003 | 23:00 | 36.1 | 36.6 | 35.4 | 91.90 | 0.00 |
| 12/15/2003 | | 35.4 | 35.8 | 34.8 | 89.70 | 0.00 |
| 12/15/2003 | 01:00 | 34.9 | 35.2 | 34.4 | 89.00 | 0.00 |
| 12/15/2003 | 02:00 | 34.1 | 34.9 | 33.8 | 87.70 | 0.00 |
| 12/15/2003 | 03:00 | 34.1 | 34.5 | 33.8 | 84.20 | 0.00 |
| 12/15/2003 | | 34.5 | 35.6 | 33.9 | 81.50 | 0.00 |
| 12/15/2003 | | 35.7 | 36.1 | 35.1 | 77.22 | 0.00 |
| | 06:00 | 35.7 | 36.2 | 35.1 | 78.37 | 0.00 |
| | 07:00 | 36.7 | 37.6 | 35.8 | 74.77 | 0.00 |
| 12/15/2003 | 08:00 | 38 | 38.6 | 37.2 | 73.68 | 0.00 |

TABLE B-1 (CONT'D)

| Date | Time | Average Temperature, °F | Maximum Temperature, °F | Minimum Temperature, °F | RH, | Total Precipitation, in. |
|------------|--|-------------------------------|-------------------------------|-------------------------------|-------|--------------------------------|
| 12/15/2003 | 09:00 | 39.1 | 40.0 | 38.2 | 73.16 | 0.00 |
| 12/15/2003 | The second secon | 40.1 | 40.7 | 39.6 | 71.01 | 0.00 |
| 12/15/2003 | 11:00 | 41.1 | 41.9 | 40.4 | 68.59 | 0.00 |
| 12/15/2003 | 12:00 | 41.5 | 41.9 | 41.2 | 63.75 | 0.00 |
| 12/15/2003 | 13:00 | 41.8 | 42.9 | 41.2 | 62.32 | 0.00 |
| 12/15/2003 | 14:00 | 42.6 | 43.3 | 42.2 | 58.05 | 0.00 |
| 12/15/2003 | 15:00 | 43.0 | 43.7 | 42.2 | 54.81 | 0.00 |
| 12/15/2003 | 16:00 | 42.4 | 43.7 | 41.7 | 54.73 | 0.00 |
| 12/15/2003 | 17:00 | 40.2 | 41.9 | 37.9 | 59.03 | 0.00 |
| 12/15/2003 | 18:00 | 37.7 | 38.5 | 36.7 | 64.99 | 0.00 |
| 12/15/2003 | | 36.2 | 37.2 | 35.0 | 67.78 | 0.00 |
| 12/15/2003 | | 34.8 | 35.7 | 33.4 | 70.31 | 0.00 |
| 12/15/2003 | | 33.6 | 34.6 | 32.6 | 73.66 | 0.00 |
| 12/15/2003 | | 32.7 | 33.3 | 32.0 | 76.44 | 0.00 |
| 12/15/2003 | 10,000 0,000 000 | 31.8 | 33.3 | 30.6 | 78.72 | 0.00 |
| 12/16/2003 | | 31.3 | 32.9 | 28.1 | 78.91 | 0.00 |
| 12/16/2003 | | 28.7 | 30.5 | 27.1 | 86.00 | 0.00 |
| 12/16/2003 | | 27.8 | 28.9 | 26.8 | 90.40 | 0.00 |
| 12/16/2003 | | 28.8 | 30.4 | 26.9 | 86.60 | 0.00 |
| 12/16/2003 | | 28.2 | 30.4 | 26.4 | 88.10 | 0.00 |
| 12/16/2003 | | 27.6 | 28.4 | 26.8 | 92.40 | 0.00 |
| 12/16/2003 | | 26.3 | 27.1 | 25.7 | 95.20 | 0.00 |
| 12/16/2003 | | 26.8 | 27.4 | 26.0 | 96.30 | 0.00 |
| 12/16/2003 | | 26.6 | 27.8 | 25.4 | 95.60 | 0.00 |
| 12/16/2003 | | 32.4 | 34.9 | 27.6 | 86.90 | 0.00 |
| 12/16/2003 | | 37.2 | 39.1 | 34.8 | 82.30 | 0.00 |
| 12/16/2003 | | 41.4 | 43.4 | 38.6 | 70.88 | 0.00 |
| 12/16/2003 | | 43.5 | 44.1 | 42.9 | 66.20 | 0.00 |
| 12/16/2003 | | 44.3 | 45.4 | 43.4 | 66.20 | 0.00 |
| 12/16/2003 | | 46.1 | 47.6 | 45.0 | 65.15 | 0.00 |
| 12/16/2003 | 15:00 | 46.4 | 48.2 | 45.0 | 67.75 | 0.00 |
| 12/16/2003 | | 49.8 | 51.3 | 47.8 | 58.74 | 0.00 |
| 12/16/2003 | | 47.8 | 49.4 | 46.4 | 61.51 | 0.00 |
| 12/16/2003 | | 46.3 | 47.0 | 45.5 | 66.63 | 0.00 |
| 12/16/2003 | | 45.1 | 46.1 | 44.1 | 71.10 | 0.00 |
| 12/16/2003 | | 43.7 | 44.6 | 43.1 | 77.83 | 0.00 |
| 12/16/2003 | | 44.0 | 45.4 | 43.1 | 78.12 | 0.00 |
| 12/16/2003 | | 46.3 | 48.4 | 45.1 | 75.89 | 0.00 |
| 12/16/2003 | | 49.6 | 50.5 | 48.2 | 69.92 | 0.00 |
| 12/17/2003 | | 49.9 | 50.6 | 49.4 | 69.89 | 0.00 |
| 12/17/2003 | | 50.9 | 51.6 | 50.2 | 69.16 | 0.00 |
| 12/17/2003 | | 52.0 | 53.1 | 50.9 | 71.40 | 0.00 |
| 12/17/2003 | | 51.5 | 53.0 | 50.8 | 74.87 | 0.00 |
| 12/17/2003 | 04:00 | 50.1 | 51.5 | 48.6 | 84.30 | 0.01 |
| 12/17/2003 | | 47.2 | 48.6 | 46.4 | 94.40 | 0.09 |

TABLE B-1 (CONT'D)

| Date | Time | Average Temperature, °F | Maximum Temperature, °F | Minimum Temperature, °F | RH, | Total Precipitation, in. |
|------------|---------------|-------------------------------|-------------------------------|-------------------------------|-------|--------------------------------|
| 12/17/2003 | | 47.3 | 48.3 | 46.1 | 98.10 | 0.26 |
| 12/17/2003 | | 47.9 | 48.3 | 47.6 | 98.70 | 0.26 |
| 12/17/2003 | $\overline{}$ | 48.3 | 48.6 | 47.9 | 99.10 | 0.13 |
| 12/17/2003 | | 48.8 | 49.5 | 48.3 | 99.30 | 0.04 |
| 12/17/2003 | | 49.6 | 50.2 | 49.0 | 99.40 | 0.00 |
| 12/17/2003 | 11:00 | 48.8 | 49.2 | 48.4 | 99.40 | 0.00 |
| 12/17/2003 | | 48.5 | 49.1 | 47.6 | 99.10 | 0.00 |
| 12/17/2003 | 13:00 | 46.6 | 48.0 | 43.7 | 93.60 | 0.08 |
| 12/17/2003 | | 40.6 | 43.8 | 38.6 | 90.40 | 0.03 |
| 12/17/2003 | | 37.6 | 38.9 | 35.7 | 93.00 | 0.03 |
| 12/17/2003 | | 35.3 | 36.1 | 34.5 | 96.10 | 0.05 |
| 12/17/2003 | | 36.1 | 36.7 | 35.1 | 89.20 | 0.00 |
| 12/17/2003 | 18:00 | 36.4 | 36.7 | 36.0 | 76.25 | 0.00 |
| 12/17/2003 | | 35.8 | 36.4 | 35.1 | 66.21 | 0.00 |
| 12/17/2003 | | 35.4 | 35.8 | 34.9 | 65.12 | 0.00 |
| 12/17/2003 | | 33.9 | 35.1 | 32.8 | 62.58 | 0.00 |
| 12/17/2003 | 22:00 | 32.4 | 33.2 | 31.9 | 64.76 | 0.00 |
| 12/17/2003 | 23:00 | 32.2 | 32.6 | 31.8 | 63.78 | 0.00 |
| 12/18/2003 | 00:00 | 32.5 | 33.1 | 31.9 | 63.43 | 0.00 |
| 12/18/2003 | | 32.5 | 33.1 | 31.9 | 64.09 | 0.00 |
| 12/18/2003 | 02:00 | 32.5 | 33.1 | 31.9 | 62.08 | 0.00 |
| 12/18/2003 | 03:00 | 31.9 | 32.6 | 31.3 | 64.02 | 0.00 |
| 12/18/2003 | 04:00 | 31.6 | 32.0 | 31.2 | 65.30 | 0.00 |
| 12/18/2003 | 05:00 | 32.0 | 32.4 | 31.5 | 63.12 | 0.00 |
| 12/18/2003 | | 31.8 | 32.1 | 31.4 | 63.84 | 0.00 |
| 12/18/2003 | 07:00 | 31.7 | 32.4 | 31.1 | 63.07 | 0.00 |
| 12/18/2003 | 08:00 | 32.1 | 32.9 | 31.4 | 60.30 | 0.00 |
| 12/18/2003 | 09:00 | 33.1 | 33.8 | 32.4 | 58.52 | 0.00 |
| 12/18/2003 | 10:00 | 34.6 | 35.5 | 33.6 | 55.55 | 0.00 |
| 12/18/2003 | 11:00 | 34.8 | 35.7 | 34.3 | 54.04 | 0.00 |
| 12/18/2003 | 12:00 | 35.8 | 36.2 | 35.2 | 51.26 | 0.00 |
| 12/18/2003 | 13:00 | 36.3 | 37.3 | 35.2 | 49.63 | 0.00 |
| 12/18/2003 | 14:00 | 35.6 | 36.2 | 35.2 | 49.47 | 0.00 |
| 12/18/2003 | 15:00 | 35.0 | 35.5 | 34.5 | 51.00 | 0.00 |
| 12/18/2003 | 16:00 | 34.8 | 35.1 | 34.5 | 49.99 | 0.00 |
| 12/18/2003 | 17:00 | 33.8 | 35.0 | 32.6 | 52.86 | 0.00 |
| 12/18/2003 | 18:00 | 31.7 | 32.8 | 30.4 | 58.79 | 0.00 |
| 12/18/2003 | 19:00 | 31.0 | 31.9 | 30.1 | 60.54 | 0.00 |
| 12/18/2003 | | 30.2 | 30.9 | 29.5 | 63.83 | 0.00 |
| 12/18/2003 | | 30.1 | 30.9 | 29.4 | 61.92 | 0.00 |
| 12/18/2003 | 22:00 | 30.6 | 31.4 | 29.8 | 59.66 | 0.00 |
| 12/18/2003 | | 30.7 | 31.2 | 30.1 | 59.11 | 0.00 |
| 12/19/2003 | | 30.6 | 31.2 | 29.9 | 59.41 | 0.00 |
| 12/19/2003 | | 29.9 | 30.5 | 29.3 | 60.87 | 0.00 |
| 12/19/2003 | 02:00 | 29.7 | 30.4 | 29.0 | 62.55 | 0.00 |

TABLE B-1 (CONT'D)

| Date | Time | Average Temperature, °F | Maximum Temperature, °F | Minimum Temperature, °F | RH, | Total Precipitation, in. |
|------------|-------|-------------------------------|-------------------------------|-------------------------------|-------|--------------------------------|
| 12/19/2003 | 03:00 | 30.3 | 30.7 | 29.9 | 62.61 | 0.00 |
| 12/19/2003 | 04:00 | 30.3 | 30.7 | 29.9 | 63.29 | 0.00 |
| 12/19/2003 | 05:00 | 30.3 | 30.7 | 29.9 | 64.17 | 0.00 |
| 12/19/2003 | 06:00 | 30.4 | 30.8 | 30.0 | 64.72 | 0.00 |
| 12/19/2003 | 07:00 | 30.2 | 30.6 | 29.9 | 65.97 | 0.00 |
| 12/19/2003 | 08:00 | 30.5 | 31.2 | 30.0 | 66.19 | 0.00 |
| 12/19/2003 | 09:00 | 31.6 | 32.6 | 30.8 | 65.79 | 0.00 |
| 12/19/2003 | 10:00 | 33.2 | 34.4 | 32.1 | 65.26 | 0.00 |
| 12/19/2003 | 11:00 | 35.4 | 36.4 | 34.2 | 62.79 | 0.00 |
| 12/19/2003 | 12:00 | 36.0 | 37.2 | 35.0 | 62.30 | 0.00 |
| 12/19/2003 | 13:00 | 35.3 | 36.8 | 34.4 | 63.81 | 0.00 |
| 12/19/2003 | 14:00 | 35.8 | 36.7 | 35.0 | 60.84 | 0.00 |
| 12/19/2003 | 15:00 | 35.9 | 36.7 | 35.2 | 60.52 | 0.00 |
| 12/19/2003 | 16:00 | 35.4 | 36.1 | 34.8 | 61.37 | 0.00 |
| 12/19/2003 | 17:00 | 34.0 | 35.0 | 33.3 | 65.68 | 0.00 |
| 12/19/2003 | 18:00 | 32.4 | 33.7 | 31.2 | 70.30 | 0.00 |
| 12/19/2003 | 19:00 | 31.0 | 31.6 | 30.4 | 74.84 | 0.00 |
| 12/19/2003 | 20:00 | 30.8 | 31.2 | 30.5 | 77.28 | 0.00 |
| 12/19/2003 | 21:00 | 30.7 | 31.1 | 30.3 | 79.10 | 0.00 |
| 12/19/2003 | 22:00 | 30.3 | 30.8 | 29.9 | 81.00 | 0.00 |
| 12/19/2003 | 23:00 | 30.1 | 30.7 | 29.4 | 81.90 | 0.00 |

APPENDIX C. SOIL MOISTURE

Daily Soil Moisture Logs

Demonstrator: Shaw, Inc.

Date: 8 December 2003

Times: No Readings (AM), 1400 (PM)

| Probe Location | Layer, in. | AM Reading, % | PM Reading, % |
|-----------------------|------------|---------------|---------------|
| Wet Area | 0 to 6 | No Readings | No Readings |
| į. | 6 to 12 | | |
| | 12 to 24 | | |
| | 24 to 36 | | |
| | 36 to 48 | | |
| Wooded Area | 0 to 6 | No Readings | No Readings |
| | 6 to 12 | | |
| | 12 to 24 | | |
| | 24 to 36 | | |
| | 36 to 48 | | |
| Open Area | 0 to 6 | No Readings | No Readings |
| | 6 to 12 | | |
| | 12 to 24 | | |
| | 24 to 36 | | |
| | 36 to 48 | | |
| Calibration Lanes | 0 to 6 | No Readings | 39.5 |
| | 6 to 12 | | 36.3 |
| | 12 to 24 | | 7.7_ |
| | 24 to 36 | | 5.6 |
| | 36 to 48 | | 5.8 |
| Blind Grid/Moguls | 0 to 6 | No Readings | No Readings |
| | 6 to 12 | | |
| | 12 to 24 | | |
| | 24 to 36 | | |
| | 36 to 48 | | |

Date: 9 December 2003

Times: 0800 (AM), 1400(PM)

| Probe Location | Layer, in. | AM Reading, % | PM Reading, % |
|-----------------------|------------|---------------|---------------|
| Wet Area | 0 to 6 | 88.2 | 88.0 |
| | 6 to 12 | 78.3 | 78.7 |
| | 12 to 24 | 69.7 | 69.9 |
| | 24 to 36 | 52.8 | 53.3 |
| 1 | 36 to 48 | 49.9 | 50.5 |
| Wooded Area | 0 to 6 | No Readings | No Readings |
| | 6 to 12 | | |
| | 12 to 24 | | |
| | 24 to 36 | | |
| | 36 to 48 | | |
| Open Area | 0 to 6 | 23.8 | 23.6 |
| | 6 to 12 | 2.1 | 2.3 |
| | 12 to 24 | 39.3 | 40.1 |
| | 24 to 36 | 60.2 | 60.1 |
| | 36 to 48 | 56.3 | 56.1 |
| Calibration Lanes | 0 to 6 | No Readings | No Readings |
| | 6 to 12 | | |
| | 12 to 24 | | |
| | 24 to 36 | | |
| | 36 to 48 | | |
| Blind Grid/Moguls | 0 to 6 | 3.9 | 3.8 |
| | 6 to 12 | 16.8 | 17.2 |
| | 12 to 24 | 39.2 | 39.8 |
| | 24 to 36 | 40.3 | 40.7 |
| | 36 to 48 | 41.8 | 41.9 |

Date: 10 December 2003 Times: 0900 (AM), 1400 (PM)

| Probe Location | Layer, in. | AM Reading, % | PM Reading, % |
|-----------------------|------------|---------------|---------------|
| Wet Area | 0 to 6 | 87.9 | 87.6 |
| | 6 to 12 | 78.5 | 79.1 |
| | 12 to 24 | 69.2 | 69.0 |
| | 24 to 36 | 53.2 | 53.8 |
| X | 36 to 48 | 50.1 | 50.7 |
| Wooded Area | 0 to 6 | No Readings | No Readings |
| | 6 to 12 | | |
| | 12 to 24 | | |
| | 24 to 36 | | |
| | 36 to 48 | | |
| Open Area | 0 to 6 | 23.2 | 22.9 |
| | 6 to 12 | 2.7 | 2.8 |
| | 12 to 24 | 39.2 | 39.5 |
| | 24 to 36 | 59.8 | 59.7 |
| _ | 36 to 48 | 56.2 | 56.0 |
| Calibration Lanes | 0 to 6 | No Readings | No Readings |
| | 6 to 12 | | |
| | 12 to 24 | | |
| | 24 to 36 | | |
| | 36 to 48 | | |
| Blind Grid/Moguls | 0 to 6 | No Readings | No Readings |
| | 6 to 12 | | 1 |
| | 12 to 24 | | |
| | 24 to 36 | | |
| | 36 to 48 | | |

Date: 11 December 2003 Times: 0800 (AM), 1415 (PM)

| Probe Location | Layer, in. | AM Reading, % | PM Reading, % |
|-----------------------|------------|---------------|---------------|
| Wet Area | 0 to 6 | 86.8 | 86.8 |
| | 6 to 12 | 79.2 | 79.5 |
| | 12 to 24 | 69.8 | 69.2 |
| | 24 to 36 | 54.7 | 55.3 |
| У. | 36 to 48 | 50.9 | 51.3 |
| Wooded Area | 0 to 6 | No Readings | No Readings |
| | 6 to 12 | | |
| | 12 to 24 | | |
| | 24 to 36 | | |
| | 36 to 48 | | |
| Open Area | 0 to 6 | 23.0 | 23.0 |
| | 6 to 12 | 2.9 | 3.1 |
| | 12 to 24 | 39.7 | 40.2 |
| | 24 to 36 | 60.1 | 60.3 |
| | 36 to 48 | 57.1 | 58.2 |
| Calibration Lanes | 0 to 6 | No Readings | No Readings |
| | 6 to 12 | | |
| | 12 to 24 | | |
| | 24 to 36 | | |
| | 36 to 48 | | |
| Blind Grid/Moguls | 0 to 6 | No Readings | No Readings |
| | 6 to 12 | | |
| | 12 to 24 | | |
| | 24 to 36 | | |
| | 36 to 48 | | |

Date: 12 December 2003 Times: 0800 (AM), 1400(PM)

| Probe Location | Layer, in. | AM Reading, % | PM Reading, % | |
|-----------------------|------------|---------------|---------------|--|
| Wet Area | 0 to 6 | 86.7 | 86.5 | |
| | 6 to 12 | 79.8 | 79.5 | |
| | 12 to 24 | 70.1 | 70.3 | |
| | 24 to 36 | 55.2 | 55.8 | |
| ¥. | 36 to 48 | 52.1 | 52.7 | |
| Wooded Area | 0 to 6 | No Readings | No Readings | |
| | 6 to 12 | | | |
| | 12 to 24 | | | |
| | 24 to 36 | | | |
| | 36 to 48 | | | |
| Open Area | 0 to 6 | 23.8 | 23.7 | |
| | 6 to 12 | 3.3 | 3.4 | |
| | 12 to 24 | 39.2 | 39.7 | |
| | 24 to 36 | 61.1 | 61.0 | |
| | 36 to 48 | 57.3 | 57.9 | |
| Calibration Lanes | 0 to 6 | No Readings | No Readings | |
| | 6 to 12 | | | |
| | 12 to 24 | | | |
| | 24 to 36 | | | |
| | 36 to 48 | | | |
| Blind Grid/Moguls | 0 to 6 | No Readings | No Readings | |
| | 6 to 12 | | 1000 | |
| | 12 to 24 |] | | |
| | 24 to 36 | | | |
| | 36 to 48 | | | |

Date: 13 December 2003 Times: 0800 (AM), 1400 (PM)

| Probe Location | Layer, in. | AM Reading, % | PM Reading, % |
|-------------------|------------|---------------|---------------|
| Wet Area | 0 to 6 | 88.2 | 88.0 |
| | 6 to 12 | 79.3 | 79.2 |
| | 12 to 24 | 70.3 | 70.2 |
| | 24 to 36 | 55.1 | 58.6 |
| | 36 to 48 | 52.3 | 52.7 |
| Wooded Area | 0 to 6 | No Readings | No Readings |
| | 6 to 12 | | |
| | 12 to 24 | | |
| | 24 to 36 | | |
| | 36 to 48 | | |
| Open Area | 0 to 6 | 23.1 | 23.0 |
| | 6 to 12 | 3.6 | 3.8 |
| | 12 to 24 | 39.3 | 39.7 |
| | 24 to 36 | 61.8 | 61.6 |
| | 36 to 48 | 57.5 | 57.8 |
| Calibration Lanes | 0 to 6 | No Readings | No Readings |
| | 6 to 12 | | |
| | 12 to 24 | | |
| | 24 to 36 | | |
| | 36 to 48 | | |
| Blind Grid/Moguls | 0 to 6 | No Readings | No Readings |
| | 6 to 12 | | |
| | 12 to 24 | | |
| | 24 to 36 | | |
| | 36 to 48 | | |

Date: 15 December 2003 Times: 0800 (AM), 1400 (PM)

| Probe Location: | Layer, in. | AM Reading, % | PM Reading, % | | | | |
|-------------------|------------|---------------|---------------|--|--|--|--|
| Wet Area | 0 to 6 | 88.7 | 88.6 | | | | |
| | 6 to 12 | 79.2 | 79.0 | | | | |
| | 12 to 24 | 70.5 | 70.7 | | | | |
| | 24 to 36 | 55.3 | 55.6 | | | | |
| ¥ . | 36 to 48 | 52.3 | 52.4 | | | | |
| Wooded Area | 0 to 6 | 79.3 | 79.7 | | | | |
| | 6 to 12 | 68.3 | 69.7 | | | | |
| | 12 to 24 | 93.4 | 93.8 | | | | |
| | 24 to 36 | 67.6 | 68.2 | | | | |
| | 36 to 48 | 58.3 | 58.8 | | | | |
| Open Area | 0 to 6 | 23.2 | 23.2 | | | | |
| | 6 to 12 | 3.4 | 3.3 | | | | |
| | 12 to 24 | 39.2 | 39.5 | | | | |
| | 24 to 36 | 60.9 | 60.9 | | | | |
| | 36 to 48 | 58.1 | 58.3 | | | | |
| Calibration Lanes | 0 to 6 | No Readings | No Readings | | | | |
| | 6 to 12 | | | | | | |
| | 12 to 24 | | | | | | |
| | 24 to 36 | | | | | | |
| | 36 to 48 | | | | | | |
| Blind Grid/Moguls | 0 to 6 | No Readings | No Readings | | | | |
| | 6 to 12 | | | | | | |
| | 12 to 24 |] | | | | | |
| | 24 to 36 | | | | | | |
| | 36 to 48 | 200 | | | | | |

Date: 16 December 2003 Times: 0800 (AM), 1400 (PM)

| Probe Location: | Layer, in. | AM Reading, % | PM Reading, % | | | | |
|------------------------|------------|---------------|---------------|--|--|--|--|
| Wet Area | 0 to 6 | 89.3 | 89.1 | | | | |
| | 6 to 12 | 79.5 | 79.4 | | | | |
| | 12 to 24 | 71.3 | 71.7 | | | | |
| | 24 to 36 | 55.7 | 55.9 | | | | |
| 3 | 36 to 48 | 55.2 | 53.1 | | | | |
| Wooded Area | 0 to 6 | 79.9 | 80.0 | | | | |
| | 6 to 12 | 70.1 | 69.9 | | | | |
| | 12 to 24 | 94.3 | 94.7 | | | | |
| | 24 to 36 | 68.7 | 68.5 | | | | |
| | 36 to 48 | 58.9 | 58.8 | | | | |
| Open Area | 0 to 6 | 23.0 | 23.1 | | | | |
| | 6 to 12 | 3.9 | 3.8 | | | | |
| | 12 to 24 | 39.3 | 39.6 | | | | |
| | 24 to 36 | 61.2 | 61.7 | | | | |
| | 36 to 48 | 58.3 | 58.5 | | | | |
| Calibration Lanes | 0 to 6 | No Readings | No Readings | | | | |
| | 6 to 12 | | | | | | |
| | 12 to 24 | | | | | | |
| | 24 to 36 | | | | | | |
| | 36 to 48 | | | | | | |
| Blind Grid/Moguls | 0 to 6 | No Readings | No Readings | | | | |
| | 6 to 12 | | | | | | |
| | 12 to 24 | | | | | | |
| | 24 to 36 | | | | | | |
| | 36 to 48 | | | | | | |

Date: 18 December 2003 Times: 0800 (AM), 1400 (PM)

| Probe Location: | Layer, in. | AM Reading, % | PM Reading, % | | | | |
|------------------------|------------|---------------|---------------|--|--|--|--|
| Wet Area | 0 to 6 | 89.3 | 89.2 | | | | |
| | 6 to 12 | 79.1 | 79.3 | | | | |
| | 12 to 24 | 69.5 | 69.7 | | | | |
| | 24 to 36 | 53.3 | 53.0 | | | | |
| ¥ | 36 to 48 | 50.5 | 50.7 | | | | |
| Wooded Area | 0 to 6 | No Readings | No Readings | | | | |
| | 6 to 12 | | | | | | |
| | 12 to 24 | | | | | | |
| | 24 to 36 | | | | | | |
| | 36 to 48 | 1 | | | | | |
| Open Area | 0 to 6 | 22.9 | 22.7 | | | | |
| | 6 to 12 | 4.3 | 4.1 | | | | |
| | 12 to 24 | 39.4 | 39.6 | | | | |
| | 24 to 36 | 61.4 | 61.3 | | | | |
| | 36 to 48 | 58.4 | 58.2 | | | | |
| Calibration Lanes | 0 to 6 | No Readings | No Readings | | | | |
| | 6 to 12 | | | | | | |
| | 12 to 24 | | 1 | | | | |
| | 24 to 36 | | | | | | |
| | 36 to 48 | | | | | | |
| Blind Grid/Moguls | 0 to 6 | No Readings | No Readings | | | | |
| | 6 to 12 | _ | | | | | |
| | 12 to 24 | | | | | | |
| | 24 to 36 | | 1 | | | | |
| | 36 to 48 | | | | | | |

Date: 19 December 2003 Times: 0800 (AM), 1400(PM)

| Probe Location: | Layer, in. | AM Reading, % | PM Reading, % |
|------------------------|------------|---------------|---------------|
| Wet Area | 0 to 6 | 88.3 | 88.1 |
| | 6 to 12 | 78.7 | 78.5 |
| | 12 to 24 | 69.8 | 70.1 |
| | 24 to 36 | 54.1 | 54.0 |
| V. | 36 to 48 | 50.7 | 50.8 |
| Wooded Area | 0 to 6 | 80.3 | 80.1 |
| | 6 to 12 | 70.2 | 70.3 |
| | 12 to 24 | 93.8 | 94.1 |
| | 24 to 36 | 68.9 | 69.2 |
| | 36 to 48 | 59.1 | 59.3 |
| Open Area | 0 to 6 | 22.5 | 22.3 |
| | 6 to 12 | 4.7 | 4.8 |
| | 12 to 24 | 39.0 | 39.0 |
| | 24 to 36 | 61.7 | 61.6 |
| | 36 to 48 | 58.6 | 58.8 |
| Calibration Lanes | 0 to 6 | No Readings | No Readings |
| | 6 to 12 | | |
| | 12 to 24 |] | 1 |
| | 24 to 36 |] | |
| | 36 to 48 | | |
| Blind Grid/Moguls | 0 to 6 | 4.1 | 4.0 |
| | 6 to 12 | 17.1 | 17.2 |
| | 12 to 24 | 39.3 | 39.3 |
| | 24 to 36 | 41.5 | 41.7 |
| | 36 to 48 | 42.1 | 42.2 |

APPENDIX D. DAILY ACTIVITY LOGS

| ditions | | MUDDY | MUDDY | MUDDY | MUDDY | мирру | MUDDY | MUDDY | MUDDY | MUDDY | MUDDY | MUDDY | МОВБУ | MUDDY | MUDDY | MUDDY | MUDDY | MUDDY | MUDDY | MUDDY |
|----------------------------------|----------------------------|----------------------|-------------------------------------|--|---------------------|--------------------|--------------------------------|--------------------|-------------------------------|--------------------|--------------|---|-------------------------------------|------------------------------------|--------------|-------------|--------------|-------------------------------|--------------------|---|
| Field Conditions | | MONS | MONS | SNOW | SNOW | SNOW | MONS | SNOW | SNOW | SNOW | SNOW | MONS | SUNNY | SUNNY MUDDY | SUNNY | SUNNY | | SUNNY | LINEAR SUNNY MUDDY | SUNNY MUDDY |
| Pottern | l mrann r | LINEAR | LINEAR | LINEAR | LINEAR | LINEAR | LINEAR | LINEAR | LINEAR | LINEAR | LINEAR | LINEAR | LINEAR | LINEAR | LINEAR | LINEAR | LINEAR | LINEAR | LINEAR | LINEAR |
| Track Method=Other Fymlein | | NA | V. | N. | AN | NA | NA A | AN | A'N | AN | NA | NA | Y X | AN A | NA | NA | AN | VA | NA | N A |
| Track | Incurrant. | LASER | LASER | LASER | LASER | LASER | LASER | LASER | LASER | LASER | LASER | LASER | LASER | LASER | LASER | LASER | LASER | LASER | LASER | LASER |
| Operational Status | ETER | INITIAL MOBILIZATION | SETUP, BEGIN DAILY OPERATIONS | CALIBRATE USING TRAILER HITCH | COLLECT DATA | COLLECT DATA | LAPTOP FAILURE, REPLACED | LUNCH/BREAK | EQUIPMENT CHECK | COLLECT DATA | COLLECT DATA | END OF OPERATIONS, EQUIPMENT BREAKDOWN | SETUP, BEGIN DAILY OPERATIONS | CALBRATE USING TRAILER HTTCH | COLLECT DATA | LUNCH/BREAK | COLLECT DATA | EQUIPMENT | COLLECT DATA | END OF OPERATIONS, EQUIPMENT BREAKDOWN |
| Onerstianal Status | SHAW BASELINE MAGNETOMETER | INITIAL MOBILIZATION | DAILY START/STOP | CALIBRATION | COLLECT DATA | COLLECT DATA | EQUIPMENT FAILURE | LUNCH/BREAK | DOWNTIME MAINTENANCE CHECK | COLLECT DATA | COLLECT DATA | DAIL-Y START/STOP | DAILY START/STOP | CALIBRATION | COLLECT DATA | LUNCH/BREAK | COLLECT DATA | DOWNTIME MAINTENANCE CHECK | COLLECT DATA | DAILY START/STOP |
| Duration, | | 124 | 06 | \script{\sint{\sint\sint\sint\sint\sint\sint\sint\sint | 25 | 30 | 30 | 30 | 15 | 5 | 85 | 45 | 55 | 15 | 45 | 40 | 0110 | 15 | 55 | 35 |
| Status Stop Time | | 1519 | 1215 | 1220 | 1245 | 1315 | 1345 | 1415 | 1430 | 1435 | 1600 | 1645 | 1055 | 1110 | 1155 | 1235 | 1425 | 1440 | 1535 | 1610 |
| Status Start Time | 2 | 1315 | 1045 | 1215 | 1220 | 1245 | 1315 | 1345 | 1415 | 1430 | 1435 | 1600 | 1000 | \$501 | 1110 | 1155 | 1235 | 1425 | 1440 | 1535 |
| Ares Tected | | CALIBRATION LANE | CALIBRATION LANE | CALIBRATION LANE | CALIBRATION LANE | BLIND TEST GRID | BLIND TEST GRID | BLIND TEST GRID | BLIND TEST GRID | BLIND TEST GRID | OPEN FIELD | OPEN FIELD | OPEN FIELD | OPEN FIELD | OPEN FIELD | OPEN FIELD | OPEN FIELD | OPEN FIELD | OPEN FIELD | OPEN FIELD |
| No. of People | 21002 | 3 | 3 | 8 | 3 | m | 3 | 3 | 3 | 3 | 3 | 3 | 4 | 4 | 4 | 4 | 4 | 4 | 4 | 4 |
| Date | Anna | 12/8/03 | 12/9/03 | 12/9/03 | 12/9/03 | 12/9/03 | 12/9/03 | 12/9/03 | 12/9/03 | 12/9/03 | 12/9/03 | 12/9/03 | 12/16/03 | 12/16/03 | 12/16/03 | 12/16/03 | 12/16/03 | 12/16/03 | 12/16/03 | 12/16/03 |

| | | λC | λ | × | X | λ | λ- | <u>></u> | <u>}</u> | λ - | χ | λ | X | |)Y | YC | λC | × | χ |
|--------------------------|--------------------|--------------------|-------------------------------------|--------------|-------------------------------|--------------|------------------------------------|---|-------------------------------------|-------------------------------------|---------------------|---------------|---------------------|----------------------------|--------------------------|--------------------|-------------------------------------|---------------------|---------------------|
| 1 | tions | MUDI | MUDE | MUDDY | MUDDY | MUDDY | МОВВУ | мирру | MUDI | MUDI | MUDI | MUDDY | MUDI | | MUDDY | MUDI | MUDI | MUDI | MUDI |
| Piest | Conditions | SUNNY MUDDY | SUNNY MUDDY | SUNNY | SUNNY | SUNNY | SUNNY | SUNNY | LINEAR CLOUDY MUDDY | LINEAR CLOUDY MUDDY | LINEAR CLOUDY MUDDY | LINEAR CLOUDY | LINEAR CLOUDY MUDDY | | LINEAR CLOUDY | INEAR CLOUDY MUDDY | LINEAR CLOUDY MUDDY | LINEAR CLOUDY MUDDY | LINEAR CLOUDY MUDDY |
| | Pattern | LINEAR | LINEAR | LINEAR | LINEAR | LINEAR | LINEAR | LINEAR | LINEAR | LINEAR | LINEAR | LINEAR | LINEAR | | LINEAR | LINEAR | LINEAR | LINEAR | LINEAR |
| Track Method-Other | Explain | NA | NA | NA. | AN | NA | NA | Ϋ́ V | NA | VA V | NA | Ϋ́Z | AN | | NA | AN | NA V | AN | NA |
| Troot | Method | LASER | LASER | LASER | LASER | LASER | LASER | LASER | LASER | LASER | LASER | LASER | LASER | | LASER | LASER | LASER | LASER | LASER |
| Onomational Status Track | - Comments | SETUP, BEGIN DAILY | CALIBRATE USING TRAILER HITCH | COLLECT DATA | EQUIPMENT CHECK | COLLECT DATA | CALBRATE USING TRAILER HITCH | END OF OPERATIONS, EQUIPMENT BREAKDOWN | SETUP, BEGIN DAILY OPERATIONS | CALIBRATE USING TRAILER HITCH | COLLECT DATA | COLLECT DATA | COLLECT DATA | SENSORS | SET UP TWO MAG SENSOR | COLLECT DATA | CALIBRATE USING TRAILER HITCH | COLLECT DATA | RENEW BADGES LASER |
| | Operational Status | DAILY START/STOP | CALIBRATION | COLLECT DATA | DOWNTIME MAINTENANCE CHECK | COLLECT DATA | CALBRATION | DAILY START/STOP | DAILY START/STOP | CALIBRATION | COLLECT DATA | COLLECT DATA | | BASELINE MAGNETOMETER 2 SI | DAILY START/STOP | COLLECT DATA | CALIBRATION | COLLECT DATA | DEMO/ RANGE ISSUE |
| Presetton | min | 25 | S | 100 | 01 | 80 | S | 25 | 35 | \$ | 20 | 40 | | B | 82 | 15 | S | 75 | 15 |
| Status | Time | 1255 | 1300 | 1440 | 1450 | 1610 | 1615 | 1640 | 0820 | 0825 | 0845 | 0925 | 1045 | | 1210 | 1225 | 1230 | 1345 | 1400 |
| Status | Time | 1230 | 1255 | 1300 | 1440 | 1450 | 1610 | 1615 | 0745 | 0820 | 0825 | 0845 | 0925 | | 1045 | 1210 | 1225 | 1230 | 1345 |
| | Area Tested | OPEN FIELD | OPEN FIELD | OPEN FIELD | OPEN FIELD | OPEN FIELD | OPEN FIELD | OPEN FIELD | OPEN FIELD | OPEN FIELD | OPEN FIELD | MOGUL AREA | OPEN FIELD | | SETUP | BLIND GRID | BLIND GRID | WOODED AREA | WOODED AREA |
| No. | People | 4 | 4 | 4 | 4 | 4 | 4 | 4 | 4 | 4 | 4 | 4 | 4 | | 4 | 4 | 4 | 4 | 4 |
| | Date | 12/18/03 | 12/18/03 | 12/18/03 | 12/18/03 | 12/18/03 | 12/18/03 | 12/18/03 | 12/19/03 | 12/19/03 | 12/19/03 | 12/19/03 | 12/19/03 | | 12/19/03 | 12/19/03 | 12/19/03 | 12/19/03 | 12/19/03 |

Note: Activities pertinent to this specific demonstration are indicated in highlighted text.

| | suc | AUDDY | мирру | MUDDY | | MUDDY | MUDDY | MUDDY | МОВВУ | MUDDY | MUDDY | MUDDY | MUDDY | MUDDY | MUDDY | MUDDY | мирру | MUDDY | MUDDY | MUDDY | MUDDY | MUDDY | MUDDY |
|------------------------|--------------------|----------------|-------------------------------------|----------------|--------------------|----------------------|----------------------------------|---------------------|---|--------------------|----------------------------------|--------------------|--|-------------------------------------|--|--------------|-------------------------------|--------------|-------------|--------------|-------------|--------------|-----------------------------|
| Field | Conditions | сгопру мирру | CLOUDY | CLOUDY | | SNOW | MONS | MONS | MONS | MONS | MONS | MONS | MONS | MONS | SNOW | SNOW | MONS | MONS | NONS | | | | SNOW |
| | Pattern | LINEAR | LINEAR | LINEAR | | LINEAR | LINEAR | LINEAR | LINEAR | LINEAR | LINEAR | LINEAR | LINEAR | LINEAR | LINEAR | LINEAR | LINEAR | LINEAR | LINEAR | LINEAR | LINEAR | LINEAR | LINEAR |
| Track Method=Other | Explain | NA | NA | AN | | NA | Y. | A'N | NA | NA A | NA | NA | NA | NA | NA | NA | NA | N. | NA | NA | NA | NA | NA |
| Track | Method | LASER | LASER | LASER | | LASER | LASER | LASER | LASER | LASER | LASER | LASER | LASER | LASER | LASER | LASER | LASER | LASER | LASER | LASER | LASER | LASER | LASER |
| Operational Status. | S | COLLECT DATA | CALIBRATE USING LASER TRAILER HITCH | 7 | | MOBILIZATION | CALIBRATE USING TRAILER HITCH | COLLECT DATA | END OF OPERATIONS, EQUIPMENT BREAKDOWN | | CALIBRATE USING TRAILER HITCH | | CALIBRATE USING LASER TRAILER HITCH | SETUP, BEGIN DAILY OPERATIONS | CALIBRATE USING LASER TRAILER HITCH | COLLECT DATA | EQUIPMENT CHECK | COLLECT DATA | LUNCH/BREAK | COLLECT DATA | | COLLECT DATA | RTS MALFUNCTION, RAIN |
| | Operational Status | COLLECT DATA | CALIBRATION | DEMOBILIZATION | SHAW BASELINE EM61 | INITIAL MOBILIZATION | CALIBRATION | COLLECT DATA | DAILY START/STOP | DAILY START/STOP | CALIBRATION | COLLECT DATA | CALIBRATION | DAILY START/STOP | | COLLECT DATA | DOWNTIME MAINTENANCE CHECK | COLLECT DATA | LUNCH/BREAK | COLLECT DATA | LUNCH/BREAK | COLLECT DATA | EQUIPMENT FAILURE |
| Duration. | min | 75 | 5 | 160 | | 124 | 9 | 45 | 35 | 06 | 5 | 55 | S | 09 | 5 | 100 | 15 | 45 | 30 | 30 | 45 | 45 | 25 |
| Status | Time | 1515 | 1520 | 1800 | | 1519 | 1525 | 1610 | 1645 | 940 | 945 | 1040 | 1045 | 845 | 850 | 1030 | 1045 | 1130 | 1200 | 1230 | 1315 | 1400 | 1425 |
| Status | Time | 1400 | 1515 | 1520 | | 1315 | 1519 | 1525 | 1610 | 810 | 046 | 945 | 1040 | 745 | 845 | 850 | 0801 | 1045 | 1130 | 1200 | 1230 | 1315 | 1400 |
| | Area Tested | WOODED AREA | WOODED AREA | WOODED | | CALIBRATION LANE | CALIBRATION LANE | CALIBRATION LANE | CALIBRATION LANE | BLIND TEST GRID | BLIND TEST GRID | BLIND TEST GRID | BLIND TEST GRID | OPEN FIELD | OPEN FIELD | OPEN FIELD | OPEN FIELD | OPEN FIELD | OPEN FIELD | OPEN FIELD | OPEN FIELD | OPEN FIELD | OPEN FIELD |
| o So | People | 4 | 4 | 4 | | е | 3 | 6 | 3 | 3 | 3 | 6 | 3 | 8 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 |
| | Date | 12/19/03 | 12/19/03 | 12/19/03 | | 12/8/03 | 12/8/03 | 12/8/03 | 12/8/03 | 12/9/03 | 12/9/03 | 12/9/03 | 12/9/03 | 12/10/03 | 12/10/03 | 12/10/03 | 12/10/03 | 12/10/03 | 12/10/03 | 12/10/03 | 12/10/03 | 12/10/03 | 12/10/03 |

Note: Activities pertinent to this specific demonstration are indicated in highlighted text

| Status Status Start Stop Du |
|--|
| Time Time |
| OPEN FIELD 1425 1500 35 |
| |
| OPEN FIELD 810 840 30 |
| OPEN FIELD 840 845 5 |
| OPEN FIELD 845 1110 145 |
| 1110 1115 |
| OPEN FIELD 1115 1125 10 DOWNTIME MAINTENANCE CHECK |
| 1125 |
| OPEN FIELD 1155 1340 105 |
| 1340 1420 |
| _ |
| OPEN FIELD 1540 1545 5 |
| OPEN FIELD 1545 1615 30 DAILY START/STOP |
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| 740 |
| 815 1005 110 |
| OPEN FIELD 1005 1135 90 EQUIPMENT FAILURE |
| 1135 |
| 1210 |
| OPEN FIELD 1335 1345 10 DOWNTIME MAINTENANCE CHECK |
| OPEN FIELD 1345 1515 90 |
| OPEN FIELD 1515 1530 15 DOWNTIME MAINTENANCE CHECK |
| OPEN FIELD 1530 1545 15 |

| Method | 01 | Status | Status | | | | | Operational | | Track | | į | |
|--|---|-----------------------|--------|----|----------|---------------|-------------------------------|---|----------|--------------|--------|--------|--------|
| CALIBRATE USING LASER NA LINEAR RAIN END OF OPERATIONS, EQUIPMENT BREAKDOWN SETUR, BEGIN LASER CALIBRATE USING CALIBRATE USING LASER NA LINEAR SUNNY COLLECT DATA LASER NA LINEAR SUNNY CALIBRATE USING COULECT DATA COULCT DATA C | A see Total Time | A see Total Time | Stop | 97 | חתנ | ation, | Constituted States | Status - | - 1 | Method=Other | 4 | Fiel | |
| TRAILER HITCH END OF OPERATIONS, EQUIPMENT BREAKDOWN SETUP, BEGIN DALLY OPERATIONS CALIBRATE USING COLLECT DATA CALIBRATE COLUDY COLLECT DATA CALIBRATE COLUDY COLLECT DATA CALIBRATE COLUDY COLLECT DATA CALIBRATE COLUDY CALIBRATE COLUDY COLLECT DATA CALIBRATE COLUDY CALIBRATE COLUDY COLLECT DATA CALIBRATE COLUDY CALIBRATE CALIBRATE CALIBRATE CALIBRATE CALIBRATE COLUDY CALIBRATE CALIBRATE CALIBRATE CALIBRATE CALIB | 11me | OPEN FIFT D 1545 1550 | 1550 | | um y | | CALIBRATION | CAI IRRATETIONG | I ASER | Explain | LINEAR | ≣۱ | MITON |
| END OF END OF END OF END OFERATIONS, EQUIPMENT BREAKDOWN SETUP, BEGIN CALLBRATE USING LASER COLLECT DATA LUNCH/BREAK LASER NA LUNCARRETE USING CALBRATE USING TRAILER HTCH COLLECT DATA LASER NA LINEAR SUNNY CALBRATE USING LASER NA LINEAR COLLECT DATA COLLECT DATA LASER NA LINEAR CLOUDY SETUP, MOVE RTS LASER NA LINEAR CLOUDY COLLECT DATA LASER NA LINEAR CLOUDY SETUP, MOVE RTS LASER NA LINEAR CLOUDY COLLECT DATA LASER NA LINEAR CLOUDY CLOUDY COLLECT DATA LASER NA LINEAR CLOUDY | | 555 | 000 | |) | _ | | TRAILER HITCH | Vince in | V. | LEALON | | I COOL |
| OPERATIONS, EQUIPMENT BREAKDOWN SETUP, BEGIN CALIBRATE USING LASER COLLECT DATA LUNCH/BREAK LASER COLLECT DATA LUNCH/BREAK LASER COLLECT DATA LUNCH/BREAK LASER COLLECT DATA C | 4 OPEN FIELD 1550 1615 25 | 1550 1615 | 1615 | _ | 25 | | DAILY START/STOP | END OF | LASER | NA | LINEAR | RAIN | MUDDY |
| SETUP, BEGIN DAILY OPERATIONS CALIBRATE USING TRAILER HTCH COLLECT DATA LASER DATA CHECK LASER COLLECT DATA LASER CALIBRATE USING TRAILER HTCH COLLECT DATA LASER NA LINEAR CLOUDY TRAILER HTCH COLLECT DATA LASER NA LINEAR CLOUDY SET UP, MOVE RTS LASER NA LINEAR CLOUDY COLLECT DATA LASER NA LINEAR CLOUDY CLOUDY CLOUDY CLOUDY COLLECT DATA LASER NA LINEAR CLOUDY CLOUDY COLLECT DATA LASER NA LINEAR CLOUDY CLOU | | | | | | | | OPERATIONS, EQUIPMENT BREAKDOWN | | | | | |
| CALIBRATE USING LASER NA LINEAR SUNNY CALIBRATE USING LASER NA LINEAR SUNNY COLLECT DATA LASER NA LINEAR SUNNY CALIBRATE USING LASER NA LINEAR SUNNY COLLECT DATA LASER NA LINEAR SUNNY PREAKDOWN SETUP, BEGIN LASER NA LINEAR CLOUDY CALIBRATE USING LASER NA LINEAR CLOUDY TRAILER HITCH COLLECT DATA LASER NA LINEAR CLOUDY COLLECT DATA LASER NA LINEAR CLOUDY SET UP, MOVE RTS LASER NA LINEAR CLOUDY <t< td=""><td>4 OPEN FIELD 730 810 40</td><td>730 810</td><td>810</td><td></td><td>40</td><td>_</td><td>DAILY START/STOP</td><td>SETUP, BEGIN</td><td></td><td>NĀ</td><td>LINEAR</td><td>SUNNY</td><td>MUDDY</td></t<> | 4 OPEN FIELD 730 810 40 | 730 810 | 810 | | 40 | _ | DAILY START/STOP | SETUP, BEGIN | | NĀ | LINEAR | SUNNY | MUDDY |
| COLLECT DATA LASER NA LINEAR SUNNY DATA CHECK LASER NA LINEAR SUNNY COLLECT DATA LASER NA LINEAR SUNNY COLLECT DATA LASER NA LINEAR SUNNY COLLECT DATA LASER NA LINEAR SUNNY CALIBRATE USING LASER NA LINEAR SUNNY TRALER HITCH END OF LASER NA LINEAR SUNNY OPERATIONS, EQUIPMENT BREAKDOWN SETUP, BEGIN LASER NA LINEAR CLOUDY TRAILER HITCH COLLECT DATA LASER NA LINEAR CLOUDY TRAILER HITCH COLLECT DATA LASER NA LINEAR CLOUDY SET UP, MOVE RTS LASER NA LINEAR CLOUDY SET UP, MOVE RTS LASER NA LINEAR CLOUDY COLLECT DATA LASER NA LINEAR CLOUDY SET UP, MOVE RTS LASER NA LINEAR CLOUDY COLLECT DATA LASER NA LINEAR CLOUDY | 4 OPEN FIELD 810 815 5 | 810 815 | 815 | | 5 | | CALIBRATION | CALIBRATE USING TRAILER HTTCH | | NA | LINEAR | SUNNY | MUDDY |
| LUNCH/BREAK LASER NA LINEAR SUNNY COLLECT DATA LASER NA LINEAR SUNNY COLLECT DATA LASER NA LINEAR SUNNY CALBRATE USING LASER NA LINEAR SUNNY TRALER HTCH END OF LASER NA LINEAR SUNNY TRALER HTCH EQUIPMENT BREAKDOWN SETUP, BEGIN LASER NA LINEAR CLOUDY TRALER HTCH COLLECT DATA LASER NA LINEAR CLOUDY TRALER HTCH COLLECT DATA LASER NA LINEAR CLOUDY SET UP, MOVE RTS LASER NA LINEAR CLOUDY SET UP, MOVE RTS LASER NA LINEAR CLOUDY COLLECT DATA LASER NA LINEAR CLOUDY SET UP, MOVE RTS LASER NA LINEAR CLOUDY COLLECT DATA LASER NA LINEAR CLOUDY | 4 OPEN FIELD 815 950 95 | 815 950 | 950 | | 95 | - | COLLECT DATA | COLLECT DATA | LASER | NA | LINEAR | SUNNY | MUDDY |
| LUNCH/BREAK LASER NA LINEAR SUNNY COLLECT DATA LASER NA LINEAR SUNNY CHANGE BATTERY LASER NA LINEAR SUNNY COLLECT DATA LASER NA LINEAR SUNNY CALIBRATE USING LASER NA LINEAR SUNNY CALIBRATE USING LASER NA LINEAR SUNNY OPERATIONS, EQUIPMENT BEAKDOWN SETUP, BEGIN LASER NA LINEAR CLOUDY SETUP, BEGIN LASER NA LINEAR CLOUDY CALIBRATE USING LASER NA LINEAR CLOUDY COLLECT DATA LASER NA LINEAR CLOUDY SET UP, MOVE RTS LASER NA LINEAR CLOUDY COLLECT DATA LASER NA LINEAR CLOUDY COLLECT DATA LASER NA LINEAR CLOUDY COLLECT DATA LASER NA LINEAR CLOUDY | 4 OPEN FIELD 950 1140 110 | 950 1140 | 1140 | | 110 | | DOWNTIME MAINTENANCE CHECK | DATA CHECK | LASER | NA. | LINEAR | SUNNY | MUDDY |
| COLLECT DATA LASER NA LINEAR SUNNY CHANGE BATTERY LASER NA LINEAR SUNNY COLLECT DATA LASER NA LINEAR SUNNY CALBRATE USING LASER NA LINEAR SUNNY CALBRATE USING LASER NA LINEAR SUNNY OPERATIONS, EQUIPMENT LASER NA LINEAR CLOUDY SETUP, BEGIN LASER NA LINEAR CLOUDY CALIBRATE USING LASER NA LINEAR CLOUDY TRAILER HITCH LASER NA LINEAR CLOUDY COLLECT DATA LASER NA LINEAR CLOUDY SET UP, MOVE RTS LASER NA LINEAR CLOUDY COLLECT DATA LASER | 4 OPEN FIELD 1140 1245 65 | 1140 1245 | 1245 | | 99 | | LUNCH/BREAK | LUNCH/BREAK | LASER | NA | LINEAR | SUNNY | MUDDY |
| CHANGE BATTERY LASER NA LINEAR SUNNY COLLECT DATA LASER NA LINEAR SUNNY CALIBRATE USING LASER NA LINEAR SUNNY CALIBRATE USING LASER NA LINEAR SUNNY OPERATIONS, EQUIPMENT LASER NA LINEAR CLOUDY SETUP, BEGIN LASER NA LINEAR CLOUDY CALIBRATE USING LASER NA LINEAR CLOUDY COLLECT DATA LASER NA LINEAR CLOUDY SET UP, MOVE RTS LASER NA LINEAR CLOUDY SET UP, MOVE RTS LASER NA LINEAR CLOUDY COLLECT DATA LASER <td>4 OPEN FIELD 1245 1430 105</td> <td>1245 1430</td> <td>1430</td> <td></td> <td>105</td> <td></td> <td>COLLECT DATA</td> <td>COLLECT DATA</td> <td>LASER</td> <td>NA</td> <td>LINEAR</td> <td>SUNNY</td> <td>MUDDY</td> | 4 OPEN FIELD 1245 1430 105 | 1245 1430 | 1430 | | 105 | | COLLECT DATA | COLLECT DATA | LASER | NA | LINEAR | SUNNY | MUDDY |
| COLLECT DATA LASER NA LINEAR SUNNY TRAILER HITCH END OF LASER NA LINEAR SUNNY OPERATIONS, EQUIPMENT BREAKDOWN SETUP, BEGIN LASER NA LINEAR CLOUDY TRAILER HITCH COLLECT DATA LASER NA LINEAR CLOUDY SET UP, MOVE RTS LASER NA LINEAR CLOUDY COLLECT DATA LASER NA LINEAR CLOUDY SET UP, MOVE RTS LASER NA LINEAR CLOUDY COLLECT DATA LASER NA LINEAR CLOUDY | 4 OPEN FIELD 1430 1440 10 | 1430 1440 | 1440 | | 10 | | DOWNTIME MAINTENANCE CHECK | | | NA | LINEAR | SUNNY | Мирру |
| CALIBRATE USING LASER NA LINEAR SUNNY END OF END OF OPERATIONS, EQUIPMENT BREAKDOWN SETUP, BEGIN TRAILER HITCH COLLECT DATA LUNCH/BREAK COLLECT DATA LASER NA LINEAR COLLECT DATA LASER NA LINEAR CLOUDY LUNCH/BREAK LASER NA LINEAR CLOUDY LUNCH/BREAK LASER NA LINEAR CLOUDY COLLECT DATA LASER NA LINEAR CLOUDY | 4 OPEN FIELD 1440 1540 60 | 1440 1540 | 1540 | _ | 09 | | COLLECT DATA | COLLECT DATA | LASER | NA | LINEAR | SUNNY | MUDDY |
| END OF | 4 OPEN FIELD 1540 1545 5 | 1540 1545 | 1545 | | 2 | | CALIBRATION | CALIBRATE USING TRAILER HITCH | LASER | NA | LINEAR | SUNNY | МОВВУ |
| SETUP, BEGIN LASER NA LINEAR CLOUDY CALIBRATE USING LASER NA LINEAR CLOUDY TRAILER HITCH COLLECT DATA LASER NA LINEAR CLOUDY LUNCH/BREAK LASER NA LINEAR CLOUDY SET UP, MOVE RTS LASER NA LINEAR CLOUDY COLLECT DATA LASER NA LINEAR CLOUDY | 4 OPEN FIELD 1545 1610 35 | 1545 1610 | 1610 | | 35 | | DAILY START/STOP | END OF OPERATIONS, EQUIPMENT BREAKDOWN | LASER | A'N | LINEAR | SUNNY | мирру |
| CALIBRATE USING LASER NA LINEAR CLOUDY TRAILER HITCH COLLECT DATA LASER NA LINEAR CLOUDY LUNCH/BREAK LASER NA LINEAR CLOUDY SET UP, MOVE RTS LASER NA LINEAR CLOUDY COLLECT DATA LASER NA LINEAR CLOUDY COLLECT DATA LASER NA LINEAR CLOUDY COLLECT DATA LASER NA LINEAR CLOUDY | 4 OPEN FIELD 910 935 25 | 910 935 | 935 | | 25 | | DALLY START/STOP | SETUP, BEGIN DAILY OPERATIONS | _ | NA | LINEAR | CLOUDY | MUDDY |
| COLLECT DATA LASER NA LINEAR CLOUDY LUNCH/BREAK LASER NA LINEAR CLOUDY SET UP, MOVE RTS LASER NA LINEAR CLOUDY COLLECT DATA LASER NA LINEAR CLOUDY COLLECT DATA LASER NA LINEAR CLOUDY COLLECT DATA LASER NA LINEAR CLOUDY | 4 OPEN FIELD 935 940 5 | 935 940 | 940 | | 5 | | CALIBRATION | CALIBRATE USING TRAILER HITCH | LASER | NA | LINEAR | CLOUDY | Мирру |
| LUNCH/BREAK LASER NA LINEAR CLOUDY SET UP, MOVE RTS LASER NA LINEAR CLOUDY COLLECT DATA LASER NA LINEAR CLOUDY COLLECT DATA LASER NA LINEAR CLOUDY COLLECT DATA LASER NA LINEAR CLOUDY | 4 OPEN FIELD 940 1115 95 | 940 1115 | 1115 | | 56 | | COLLECT DATA | COLLECT DATA | LASER | NA | LINEAR | CLOUDY | MUDDY |
| SET UP, MOVE RTS LASER NA LINEAR CLOUDY COLLECT DATA LASER NA LINEAR CLOUDY COLLECT DATA LASER NA LINEAR CLOUDY | 1115 | 1115 1140 | 1140 | | 25 | | LUNCH/BREAK | LUNCH/BREAK | LASER | NA | LINEAR | CLOUDY | MUDDY |
| COLLECT DATA LASER NA LINEAR CLOUDY COLLECT DATA LASER NA LINEAR CLOUDY | 4 OPEN FIELD 1140 1230 50 | 1140 1230 | 1230 | | 95 | $\overline{}$ | DAILY START/STOP | SET UP, MOVE RTS | LASER | NA | LINEAR | CLOUDY | MUDDY |
| COLLECT DATA LASER NA LINEAR CLOUDY | D 1230 1240 | 1230 1240 | 1240 | | 10 | | COLLECT DATA | COLLECT DATA | LASER | NA | LINEAR | CLOUDY | MUDDY |
| | 4 WOODED 1240 1400 100 AREA 1240 100 | 1240 1400 | 1400 | _ | <u>8</u> | | COLLECT DATA | COLLECT DATA | LASER | NA V | LINEAR | CLOUDY | Мирру |

| | | | ~ | 15 | _ | 5 | <u></u> | S | 15 | 154 | 15 | N | <u> </u> | ~ | <u> </u> | 1 | N. |
|-------------|--------------|--------------------|----------------------------------|----------------|--|-------------------------------|----------------|------------------|----------------|-------------------------------|----------------------------------|--------------|-------------|------------------|--------------|-------------|----------------|
| | þ | ions | MUDD | MUDD | Мирру | MUDD | Каалы | MUDD | МОДДУ | MUDDY | MUDD | Мирру | Мирру | М ОВРУ | МИВВУ | MUDDY | MUDDY |
| | Field | Conditions | СТОПВУ МИВВУ | сголру мирру | сгопрх | стопру мирру | сгоиру мирру | стопру мирру | CLOUDY | SUNNY | SUNNY MUDDY | SUNNY | SUNNY | SUNNY | SUNNY | SUNNY | сголру мирру |
| | | Pattern | LINEAR | LINEAR | LINEAR | LINEAR | LINEAR | LINEAR | LINEAR | LINEAR | LINEAR | LINEAR | LINEAR | LINEAR | LINEAR | LINEAR | LINEAR |
| Track | Method=Other | Explain | NA V | NA | , VA | NA | AN | NA | AN | NA | NA | NA V | NA | NA | AN | Ϋ́ | Y. |
| | Track | Method | LASER | LASER | LASER | LASER | LASER | LASER | LASER | LASER | LASER | LASER | LASER | LASER | LASER | LASER | LASER |
| Operational | Status - | Comments | CHANGE BATTERY | COLLECT DATA | END OF OPERATIONS, LASER EQUIPMENT BREAKDOWN | SETUP, BEGIN DAILY OPERATIONS | COLLECT DATA | SETUP, MOVE RTS | COLLECT DATA | SETUP, BEGIN DAILY OPERATIONS | CALIBRATE USING TRAILER HITCH | COLLECT DATA | LUNCH/BREAK | SETUP, MOVE RTS | COLLECT DATA | LUNCH/BREAK | DEMOBILIZATION |
| | | Operational Status | DOWNTIME MAINTENANCE CHECK | COLLECT DATA | DAILY START/STOP | DAILY START/STOP | COLLECT DATA | DAILY START/STOP | COLLECT DATA | DAILY START/STOP | CALIBRATION | COLLECT DATA | LUNCH/BREAK | DAILY START/STOP | COLLECT DATA | LUNCH/BREAK | DEMOBILIZATION |
| | Duration, | min | 30 | 75 | 20 | 70 | 55 | 15 | 10 | 09 | 5 | 08 | 15 | 30 | 70 | 40 | 160 |
| Status | | Time | 1430 | 1545 | 1605 | 840 | 935 | 950 | 0001 | 830 | 835 | 955 | 1010 | 1040 | 1150 | 1230 | 1800 |
| Status | Start | Time | 1400 | 1430 | 1545 | 730 | 840 | 935 | 950 | 730 | 830 | 835 | 556 | 1010 | 1040 | 1150 | 1520 |
| | | Area Tested | WOODED AREA | WOODED AREA | WOODED AREA | WOODED AREA | WOODED AREA | WOODED AREA | WOODED AREA | MOGUL AREA | MOGUL AREA | MOGUL | MOGUL | MOGUL AREA | MOGUL | MOGUL | MOGUL AREA |
| No. | Jo | People | 4 | 4 | 4 | 4 | 4 | 4 | 4 | 4 | 4 | 4 | 4 | 4 | 4 | 4 | 4 |
| | | Date | 12/15/03 | 12/15/03 | 12/15/03 | 12/16/03 | 12/16/03 | 12/16/03 | 12/16/03 | 12/18/03 | 12/18/03 | 12/18/03 | 12/18/03 | 12/18/03 | 12/18/03 | 12/18/03 | 12/19/03 |

APPENDIX E. REFERENCES

- 1. Standardized UXO Technology Demonstration Site Handbook, DTC Project No. 8-CO-160-000-473, Report No. ATC-8349, March 2002.
- 2. Aberdeen Proving Ground Soil Survey Report, October 1998.
- 3. Data Summary, UXO Standardized Test Site: APG Soils Description, May 2002.
- 4. Practical Nonparametric Statistics, W.J. Conover, John Wiley & Sons, 1980, Pages 144 to 151

APPENDIX F. ABBREVIATIONS

AEC = U.S. Army Environmental Center

APG = Aberdeen Proving Ground

ASCII = American Standard Code for Information Interchange

ATC = U.S. Army Aberdeen Test Center

EQT = U.S. Army Environmental Quality Technology Program

ERDC = U.S. Army Corp of Engineers Engineering Research and Development Center

EM = electromagnetic

ESTCP = Environmental Security Technology Certification Program

HEAT = high-explosive, antitank JPG = Jefferson Proving Ground

POC = point of contact
QA = quality assurance
OC = quality control

ROC = receiver-operating characteristic

RTS = robotic total station

SERDP = Strategic Environmental Research and Development Program

UXO = unexploded ordnance

YPG = U.S. Army Yuma Proving Ground

APPENDIX G. DISTRIBUTION LIST

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